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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered) READ INST REPORT DOCUMENTATION PAGE BEFORE COMPL 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALO 1. REPORT NUMBER 910504 TYPE OF REPORT & PERIOD COVERED 4. TITLE (and Subtitle) Phase I Dam Inspection Report Final Report National Dam Safety Program Lake Sherwood Dam (MO 10202) 6 PERFORMING ORG. NEDORT NUMBER Warren County, Missouri 8. CONTRACT OR GRANT NUMBER(#) 7. AUTHOR(a) Kenneth Balk and Associates, Inc. DACW43-78-C-Ø169 PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 9. PERFORMING ORGANIZATION NAME AND ADDRESS U.S. Army Engineer District, St. Louis Dam Inventory and Inspection Section, LMSED-PD 210 Tucker Blvd., North, St. Louis, Mo. 63101 SPORT DATE 11. CONTROLLING OFFICE NAME AND ADDRESS U.S. Army Engineer District, St. Louis January 19 Dam Inventory and Inspection Section, LMSED-PD 13 NUMBER OF PAGES 210 Tucker Blvd., North, St. Louis, Mo. 63101
14. MONITORING AGENCY NAME & ADDRESS(If different from Controlling Office) <u>Approximately 120</u> 15. SECURITY CLASS. (of this report) National Dam Safety Program. Lake UNCLASSIFIED Sherwood Dam (MO 10202), Upper 154. DECLASSIFICATION/DOWNGRADING Mississippi - Mississippi - Kaskaskia -St. Louis Basin, Warren County, Missouri 16. DI Phase I Inspection Report. Approved for release; distribution unlimited. 17. DISTRIBUTION STATEMENT (of the postract entered in Block 20, if different from Report)  $t \to V r$ 18. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Dam Safety, Lake, Dam Inspection, Private Dams ASSTRACT (Continue on reverse side if necessary and identity by block number) This report was prepared under the National Program of Inspection of Non-Federal Dams. This report assesses the general condition of the dam with respect to safety, based on available data and on visual inspection, to determine if the dam poses hazards to human life or property. DD FORM 1473 EDITION OF ! NOV 65 IS OBSOLETE

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UNCLASSIFIED



# DEPARTMENT OF THE ARMY ST. LOUIS DISTRICT, CORPS OF ENGINEERS 210 NORTH 12TH STREET ST. LOUIS, MISSOURI 63101

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SUBJECT: LAKE SHERWOOD DAM - PHASE I INSPECTION REPORT.

This report presents the results of field inspection and evaluation of the Lake Sherwood Dam.

It was prepared under the National Program of Inspection of Non-Federal Dams

This dam has been classified as unsafe, non-emergency by the St. Louis District as a result of the application of the following criteria:

- 1) Spillway will not pass 50 percent of the Probable Maximum Flood
- 2) Overtopping could result in dam failure.
- 3) Dam failure significantly increases the hazard to loss of life downstream

SUBMITTED BY:	SIGNED	10 APR 1979
30000111100 011	Chief, Engineering Division	Date
APPROVED BY:	www.thu	10 APR 1979
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## LAKE SHERWOOD DAM WARREN COUNTY, MISSOURI

MISSOURI INVENTORY NO. 10202

PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

PREPARED BY

Kenneth Balk & Associates, Inc. St. Louis, Missouri Shannon & Wilson, Inc. St. Louis, Missouri

PREPARED FOR

ST. LOUIS DISTRICT, CORPS OF ENGINEERS

JANUARY, 1979

#### PHASE I REPORT

## NATIONAL DAM SAFETY PROGRAM

Name of Dam State Located County Located Stream Date of Inspection Lake Sherwood Missouri Warren County Tributary To Wolf Creek August 25, 1978

Lake Sherwood Dam, No. 10202 was inspected using the "Recommended Guidelines for Safety Inspection of Dams". These guidelines were developed by the Chief of Engineers, U. S. Army, Washington, D.C., with the help of Federal and state agencies, professional engineering organizations, and private engineers. The resulting guidelines are considered to represent a consensus of the engineering profession.

Lake Sherwood Dam was visually inspected by an interdisciplinary team of engineers from Kenneth Balk & Associates, Inc. and Shannon & Wilson, Inc. The purpose of the inspection was to make a preliminary assessment of the general condition of the dam with respect to safety in order to determine if, in the opinion of the interdisciplinary team, the dam poses recognizable hazards to human life or property. This assessment is based solely upon data made available and visual evidence observed during the site visit.

To make a complete assessment of the safety of the dam would require detailed studies and engineering analyses beyond the scope of this preliminary assessment.

Based on the criteria in the guidelines, the dam is in the high hazard potential classification, which means that loss of life and appreciable property loss could occur in the event of failure of the dam. The estimated damage zone extends approximately five miles downstream of the dam. Within the damage zone are a wastewater treatment works, seven farm complexes with farmhouses, and one State highway crossing. Lake Sherwood Dam is in the intermediate size classification since it is greater than 40 feet high but less than 100 feet high.

The inspection and evaluation indicate that the spillway of Lake Sherwood does not meet the criteria set forth in the guidelines for a dam having the above size and hazard potential. Lake Sherwood is an Intermediate size dam with a high hazard potential, required by the guidelines to pass the PMF. The Probable Maximum Flood, (PMF) is defined as the flood discharge that may be expected from the most severe combination of critical meteorological and hydrologic

conditions that are <u>reasonably possible</u> in the region. Considering the high hazard potential to loss of life and property downstream of the dam, the outlet facilities of Lake Sherwood Dam should be able to pass the PMF without overtopping the dam. However, it was determined that the spillway will only pass approximately 20 percent of the PMF without overtopping the dam.

The evaluation of Lake Sherwood also indicated that the spillway will pass the 100-year flood; that is, a flood having a 1 percent chance of being equalled or exceeded during any given year.

Deficiencies visually observed by the inspection team included the lack of rip rap on the upstream face of the dam. Other deficiencies, in our opinion, are the lack of seepage and stability analyses comparable to the requirements of the Recommended Guidelines, and seismic stability analyses.

It is recommended that action be taken in the near future to correct or control the deficiencies described. A detailed report discussing each of these deficiencies is attached.

Ervin H. Baumeyer, P.E.

Principal-In-Charge

Kenneth Balk and Associates, Inc.

St. Louis, Missouri

Lutz Kunze, P.E.

Principal Éngineer

Shannon & Wilson, Inc.

St. Louis, Missouri



Overview of Lake and Dam

## PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM LAKE SHERWOOD DAM - ID NO. 10202

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#### SECTION 1 - PROJECT INFORMATION

#### 1.1 GENERAL

- a. <u>Authority</u>. The National Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of safety inspection of dams throughout the United States. Pursuant to the above, the St. Louis District, Corps of Engineers, District Engineer directed that a safety inspection of the Lake Sherwood Dam be made.
- b. <u>Purpose of Inspection</u>. The purpose of the inspection was to make an assessment of the general condition of the dam with respect to safety, based upon data made available and visual inspection, in order to determine if the dam poses hazards to human life or property.
- c. Evaluation Criteria. Criteria used to evaluate the dam were furnished by the Department of the Army, Office of the Chief of Engineers, in "Recommended Guidelines for Safety Inspection of Dams". These guidelines were developed with the help of several Federal agencies and many State agencies, professional engineering organizations, and private engineers.

#### 1.2 DESCRIPTION OF PROJECT

a. <u>General</u>. Lake Sherwood is located downstream of a series of five reservoirs. One of these, Lake Alan is too small to be of appreciable significance to Lake Sherwood. Lake Eleanor, a 3.7 acre impoundment, discharges into lake Marian, an 8.3 acre impoundment, which then discharges into Lake Sherwood. Both of these lakes are located to the northeast of Lake Sherwood. Sugar Hollow Lake, directly to the north of Lake Sherwood, contains a pool of approximately 15.6 acres, and discharges into Lake Sherwood. Lake Robin Hood, an 8.3 acre impoundment, lies to the northwest of Lake Sherwood and also discharges into it.

#### b. Description of Dam and Appurtenances.

- (1) The Lake Sherwood Dam is an earth structure built on Wolf Creek in the southeastern part of Warren County, Missouri. Topography adjacent to the valley is rolling to steep. Most of the area in the vicinity of the dam is covered with a residual soil overlying dolomite. Topography in the vicinity of the dam is shown on Plate 1.
- (2) The principal spillway consists of three 36x58 inch corrugated metal arch pipes laid through the right abutment. An overflow spillway, generally semi-circular in shape, is located to the right of the principal spillway with the outlet channel cut into dolomite.
- (3) Pertinent physical data are given in paragraph 1.3 below.

- c. <u>Location</u>. The dam is located in the southeastern portion of Warren County, Missouri, as shown on Plate 2. The lake formed by the dam is on the Missouri-Warren County New Melle quadrangle sheet in the SE 1/4 of Section 11, T45N, R1W.
- d. Size Classification. Criteria for determining the size classification of  $d_{\rm d}ms$  and impoundments are presented in the guidelines referenced in paragraph 1.1c above. Based on these criteria, this dam and impoundment is in the intermediate size category.
- e. <u>Hazard Classification</u>. Guidelines for determining hazard classification are presented in the same guidelines as referenced in paragraph 1.1 c. Based on referenced guidelines, the Corps of Engineers has determined that this dam is in the High Hazard Classification and thus has been selected by the Corps of Engineers for a Phase 1 inspection.
- f. Ownership. It is our understanding that this dam is owned by Lake Sherwood Estates Home Owners Association, Lake Sherwood, Mo.
  - g. Purpose of Dam. The dam forms a recreational lake.
- Design and Construction History. The dam was completed in Some engineering data and remedial construction records were available. Leaks developed in the embankment near the left abutment and grouting was performed in 1970 by Test Drilling Services, Inc., a grouting and drilling firm, located in St. Louis, Missouri. Horner & Shifrin, Inc., a St. Louis consulting Engineering firm, were consulted regarding the leakage from the left abutment and it reportedly was their opinion that the source of the water is a solution channel in the Plattin limestone. A V-notch weir was installed to measure the flow of the spring from the left abutment. The water loss is a continuing occurrence, as evidenced by a 1977 report by Dr. J. H. Williams, Chief, Applied Engineering and Urban Geology, Geology and Land Survey, State of Missouri, which states that "If the leak at Lake Sherwood is continuously monitored to assure that it remains confined to bedrock, no danger exists". According to Mr. E. Sanders, Executive Director of the Lake Sherwood Estates Home Owners Association, the flow is relatively constant at approximately 200 GPM. Both the temperature and flow of the water from the left abutment is measured at regular intervals.
- i. <u>Normal Operating Procedure</u>. Normal rainfall, runoff, transpiration, evaporation, and spillway discharges all combine to maintain a relatively stable water surface elevation.

#### 1.3 PERTINENT DATA

## a. <u>Drainage Area</u>

Direct Tributary A	<u>Ireas</u>	lotal iributary Areas
Lake Sugar Hollow Lake Robin Hood	= 462 Ac.	107 Ac. 144 Ac. 966 Ac. 462 Ac. 2937 Ac.
Lake Sherwood	=1365 Ac.	2337 AC.

## b. Discharge at Damsite.

- (1) Three 36x58 inch arch-pipes 332 c.f.s. at maximum pool.
- (2) Emergency spillway 1204 c.f.s. at maximum pool.
- (3) Estimated experienced maximum flood at damsite approximately two feet below top of dam, 522 cfs.
  - c. Elevation (U.S.G.S.)
  - (1) Top of dam 629.6 (see Plate 3).
  - (2) Spillway crest 622.8.
  - (3) Streambed at centerline of dam 560 (est.).
  - (4) Maximum tailwater unknown.
  - d. Reservoir. Length of maximum pool 5,600 feet +.
  - e. Storage (Acre-feet).

		Lake Eleanor	Lake Marian	Lake Sugar <u>Hollow</u>	Lake Robin Hood	Lake Sherwood
(1)	Normal	58	260	288	144	2400
(2)	Maximum		291	308	155	2837

- f. Reservoir Surface (Acres).
- (1) Top of dam 163
- (2) Spillway crest 141
- g. Dam.
- (1) Type earth embankment.
- (2) Length 1,000 feet.
- (3) Height 70 feet maximum.

- (4) Top width 30 feet.
- (5) Side Slopes (Measured with a slope meter/inclinometer in degrees and converted to ratios.)
  - (a) Downstream 2.6 H to 1 V.
  - (b) Upstream 3.7 H to 1 V.
  - (6) Zoning unknown
  - (7) Impervious core unknown
  - (8) Cutoff unknown
  - (9) Grout curtain unknown
  - h. <u>Diversion and Regulating Tunnel</u>. NONE
  - i. Spillway.
  - (1) Type Three 36" x 58" Corrugated Metal Arch Pipes
  - (2) Crest elevation 622.9 U.S.G.S.
  - j. Regulating Outlets. NONE
  - k. Overflow Spillway.
- (1) Type Semi Circular Weir, varying in length as water surface rises. Length at top of dam elevation is approximately 155 feet.
  - (2) Crest 625.8

#### SECTION 2 - ENGINEERING DATA

#### 2.1 DESIGN

Design data made available (for review only) consisted of one drawing depicting a cross-section of the dam.

#### 2.2 CONSTRUCTION

The dam was completed in 1967. Remedial design data relative to grouting to control seepage was available for review, and were considered in this report. Among these data were reports by Dr. J. H. Williams, Horner and Shifrin, Inc. and Test Drilling Services, Inc. as outlined in Paragraph 1.2 h.

#### 2.3 OPERATION

No records of the maximum loading on the dam were available.

#### 2.4 EVALUATION

- a. Availability. Some engineering and geological data were available for review, as discussed in Paragraphs 2.2 and 1.2 h.
- b. Adequacy. The engineering data made available was not sufficient to make a detailed assessment of the design, construction, and operation. The lack of seepage and stability analyses comparable to the requirements of the Recommended Guidelines is considered a deficiency. Remedial design data was considered adequate.
- c. <u>Validity</u>. No valid engineering data on design were available. Remedial design data was available and was considered sufficient to assess the potential problem of the flow of water from springs in the left abutment.

#### SECTION 3 - VISUAL INSPECTION

#### 3.1 FINDINGS

- a. <u>General</u>. A visual inspection of the Lake Sherwood Dam was carried out on August 25, 1978. Personnel making inspection were employees of Kenneth Balk and Associates, Inc. and Shannon and Wilson, Inc. of St. Louis and included civil, geotechnical, and structural engineers and an engineering geologist. Specific observations are discussed below.
  - b. <u>Dam</u>. The inspection team observed the following at the dam.

The dam is an earth embankment with a paved roadway crossing the crest. No detrimental settlement, depressions, cracking, erosion, animal burrows or slope instability was observed on either the embankment or the abutments. A waste-water treatment facility is located immediately downstream from the toe of the embankment. At the time of the inspection, construction of expansion facilities was underway.

Three springs were observed in the left abutment. The closest spring to the dam is located at the juncture of the toe and the left abutment. A V-notch weir has been constructed some 20 feet downstream from this spring and at the time of the inspection, this spring was flowing at 200 gallons per minute. The other two springs are some distance (200 feet plus) downstream from the juncture of the embankment and the left abutment and their flow was not measured.

A small area at the toe of the dam at the juncture of the left abutment was wet and soft, due to flow from the nearest spring. The flow from this spring has been channelized to flow over the weir. A line of grout pipes were observed on the downstream slope of the embankment near the left abutment. The downstream slope of the dam was partially mowed on the day of the inspection and there were no bushes or small trees visible on the unmowed portion, which is considered evidence of a regular, periodic vegetation control program.

- c. Appurtenant Structures. A spillway, consisting of three (3) 36x58 inch Corrugated Metal arch pipes, is located on the right abutment. A secondary or overflow spillway is located at the right of the principal spillway, in the right abutment.
- d. Reservoir Area. No wave wash, excessive erosion or slides were observed along the shore of the reservoir.

#### e. Damsite Geology.

Right Abutment. Exposed on the right abutment is a formation consisting of mainly argillaceous dolomite (Joachim Formation); yellowish-brown in color, thinly to medium bedded, with bedding almost horizontal, medium to finely crystalline. This formation is sparsely jointed with joints almost vertical to the bedding plane and strike almost NS. Thin layer of grayish-brown, clayey-silty shale is present at places. Chert nodules, light-gray in color, and quartz lenses are also present.

Spillway Outlet Channel. Spillway discharge channel is cut through the right abutment in yellowish-brown, argillaceous dolomite. There is no visual evidence of significant ercsion of the channel.

Left Abutment. Small outcrops of argillaceous dolomite are present on the left abutment. This dolomite (Joachim Formation) is mostly covered with a thick layer of reddish-brown clayey silt and is medium to finely crystalline, sparsely jointed with joints perpendicular to the bedding planes.

Joint opening = 1/6 inch to 1/2 inch

Filling material - argillaceous and calcatic

Open joints - 10%; Closed joints - 90%

Chert nodules and quartz lenses are also present at places.

#### 3.2 EVALUATION

The state of the s

Recorded monitoring on a regular schedule of the volume of the flow and the temperature of the water from the spring should be continued. The water should also be checked for clarity and if it starts to carry sediment, the situation should be reviewed with a professional engineer experienced in the design and construction of dams.

The lack of rip rap on the upstream face of the dam is considered a deficiency for a dam of this size.

#### SECTION 4 - OPERATIONAL PROCEDURES

#### 4.1 PROCEDURES

The lake level is controlled by rainfall, runoff, evaporation, and discharge through uncontrolled spillway.

#### 4.2 MAINTENANCE OF DAM

No maintenance records of the dam were available. Mowing of the downstream slope and general cleanliness, and the monitoring of the flow from the springs discussed earlier, suggest that a regular maintenance program is in effect.

#### 4.3 MAINTENANCE OF OPERATING FACILITIES

No regulating structure exists.

#### 4.4 DESCRIPTION OF ANY WARNING SYSTEM IN EFFECT

The inspection team is not aware of any existing warning system for this dam.

#### 4.5 EVALUATION

It is our opinion that the operational procedures apparently have been satisfactory notwithstanding the lack of records.

#### SECTION 5 - HYDRAULIC/HYDROLOGIC

#### **5.1 EVALUATION OF FEATURES**

- a. <u>Design Data</u>. There were no hydraulic and hydrological design data made available.
- b. Experience Data. The drainage area and lake surface area are developed from USGS New Melle, Mo. Quadrangle, 7.5 minute series, dated 1972. The spillway and dam layout are from surveys made during the inspection.

#### c. Visual Observations.

The spillways and outlet channel are in good condition. Spillway discharges will not affect the integrity of the dam.

Full cognizance of the upstream impoundments, Lakes Eleanor, Marian, Sugar Hollow, and Robin Hood, was taken in the analyses of the overtopping potential of Lake Sherwood. In this analysis, it was assumed that, while the dams of the upstream reservoirs might be overtopped, failure of their embankments would not occur.

Under this assumption, the upstream reservoirs have a beneficial effect on Lake Sherwood. At the time of the PMF peak outflow rate for Lake Sherwood, approximately 568 acre feet of water is in-storage in the four upstream reservoirs, being contained between the spillway crest elevations and the water surface elevations.

If simultaneous failure of all the upstream dams is assumed to occur at the same time as the peak rate of local runoff is entering Lake Sherwood, the effect of the upstream reservoirs would be negative on Lake Sherwood. If it is assumed that, in addition to simultaneous failure, instantaneous arrival of the flood waves occurs, then approximately 1886 acre feet of water would be entering Lake Sherwood, in addition to the local runoff. The 1886 acre feet being made up of the 568 acre feet mentioned above and approximately 1318 acre feet which is contained between the bottom of the reservoirs and the spillway crests.

It can be said that if the above failure, or something approaching such an event were to occur, the effect on Lake Sherwood would be to lessen the percentage of the PMF which can be accommodated, or in other words, to increase the overtopping potential of Lake Sherwood.

The results of the analysis of overtopping potential is as follows:

<u>Lake</u>	% PMF	Maximum Depth Over Dam (Ft)	Maximum Storage (Ac-Ft)	Peak Outflow Rate (CFS)	Duration Of Overtopping (Hrs)	Time To Peak Outflow (Hrs)
Eleanor	100	2.7	26	1802	11.2	15.83
n	50	1.6	21	902	7.0	15.83
Marian	100	2.0	53	2278	7.6	15.83
11	50	1.3	46	1091	5.4	15.92
Sugar Hollow	100	13.4	426	8540	14.2	16.42
ĭĭ	50	6.8	288	4270	10.2	16.42
Robin Hood	100	9.4	18 <b>9</b>	4811	14.5	16.17
**	50	6.0	143	2414	11.6	16.17
Sherwood	100	4.8	1833	24300	7.2	16.42
н	50	2.4	1429	11704	4.7	16.42

The lakes and spillways have been found adequate to accommodate the following.

<u>Lake</u>	% of the P.M.F. Accommodated
Eleanor	Approximately 5
Marian	Approximately 10
Sugar Hollow	Less than 5
Robin Hood	Less than 5
Sherwood	Approximately 20

For the 100 year flood, an event which has a 1% chance of being equaled or exceeded at least once in any given year, the results of the analysis indicate that the spillways of Lake Sherwood are adequate, but those of the upstream reservoirs are not.

d. Overtopping Potential. The spillway has been found to be inadequate to pass the Probable Maximum Flood (PMF) without overtopping the dam. The probable maximum flood is defined as the flood discharge that may be expected from the most severe combination of critical meteorological and hydrologic conditions that are <u>reasonably possible</u> in the region.

The estimated damage zone extends five miles downstream of the dam. Within the damage zone are a wastewater treatment works, seven farm complexes with farmhouses, and one State highway crossing.

#### SECTION 6 - STRUCTURAL STABILITY

#### 6.1 EVALUATION OF STRUCTURAL STABILITY

- a. <u>Visual Observations</u>. Visually observed conditions which can affect the structural stability of this dam have been discussed in Section 3, paragraph 3.1 b.
- b. <u>Design and Construction Data</u>. No design or construction data relating to the structural stability of the dam were found except that discussed in Section 1.2, paragraph 1.2 h.
- c. Operating Records. No records were available at the time of the inspection.
- d. <u>Post-Construction Changes</u>. No post-construction changes other than referenced in Section 1, paragraph 1.2 h exists.
- e. <u>Seismic Stability</u>. The location of Lake Sherwood Dam is in Seismic Zone 1. The engineering data available was insufficient to evaluate the seismic stability, however to our knowledge, an earthquake of the magnitude that may reasonably be expected in Seismic Zone 1 has not caused a structural collapse of a dam of this size and magnitude.

#### SECTION 7 - ASSESSMENT/REMEDIAL MEASURES

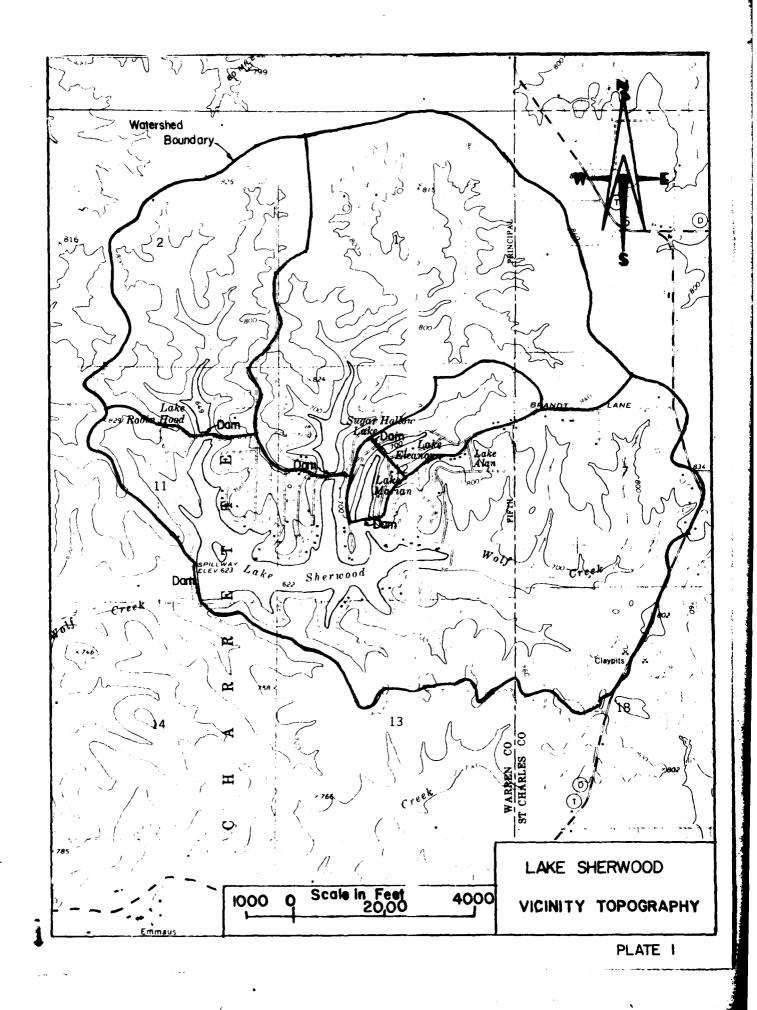
#### 7.1 DAM ASSESSMENT

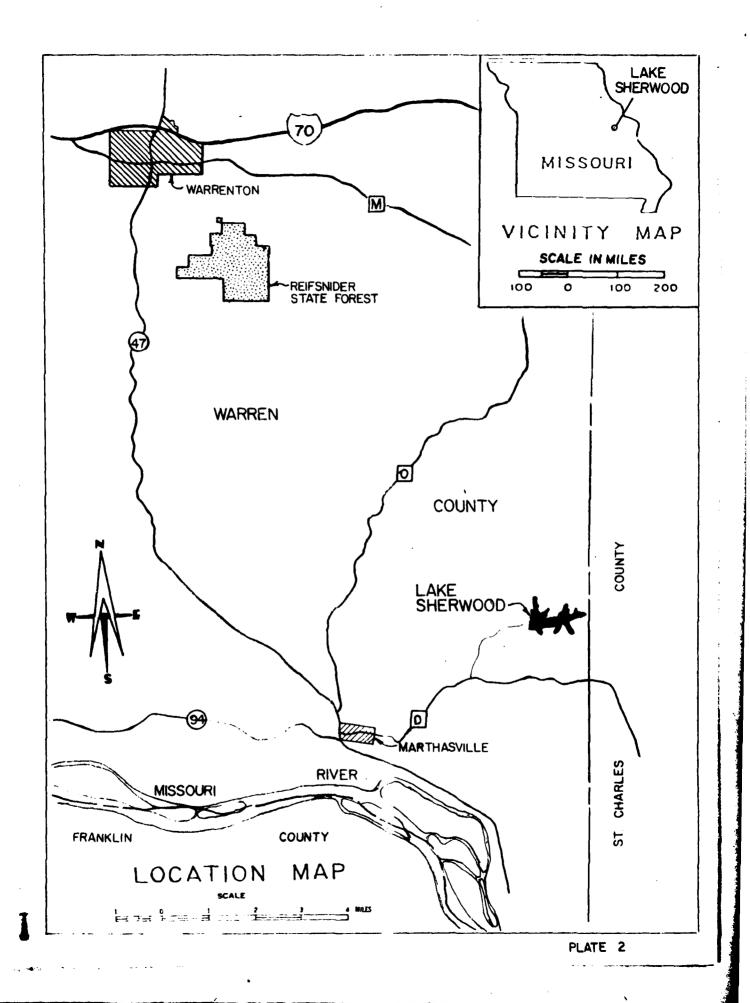
- a. <u>Safety</u>. Corrective measures, in our opinion, should be taken for the deficiencies visually observed by the inspection team, i.e. lack of rip rap on the upstream face of the embankment. The spring nearest to the dam, in the left abutment, is not in itself considered a deficiency, however, due to its location, should be monitored. Inadequate spillway capacities are also considered to be a deficiency.
- b. Adequacy of Information. Due to the lack of sufficient engineering design and construction data, except that discussed in Section 1, the conclusions of this report were based on performance and external visual conditions. The lack of seepage and stability analyses comparable to the requirements of the recommended guidelines is a deficiency which should be corrected. The inspection team considers that these data are sufficient to support the conslusions herein.
- c. <u>Urgency</u>. The deficiencies described herein are serious and corrective actions listed below should be initiated in the near future.
- d. <u>Necessity for Phase II.</u> The conclusions of this report are based on a visual inspection and review of data made available. The inspection team considers these to be sufficient to make an adequate assessment of deficiencies and therefore no Phase II inspection is recommended.

#### 7.2 REMEDIAL MEASURES

- a. The following remedial measures are recommended.
- (1) The spring nearest to the dam should be protected to prevent erosion of the toe of the embankment and the flow channelized to the weir.
- (2) Flow from the spring should be monitored on a regular schedule and periodically checked for sedimentation.
- (3) Up-to-date records of all future maintenance and repairs should be kept.
- (4) Spillway capacity and/or height of dam should be increased to pass 100 percent (100%) of the Probable Maximum Flood.
- (5) Consideration should be given to increasing the spillway capacities and/or height of dams of the upstream reservoirs.

- (6) Seepage and stability analyses should be performed by a professional engineer experienced in the design and construction of dams.
- (7) The dam should be periodically inspected by an engineer experienced in the design and construction of dams, and records kept of these inspections.





Apparent Lake Drai Sherwood (17'w. As

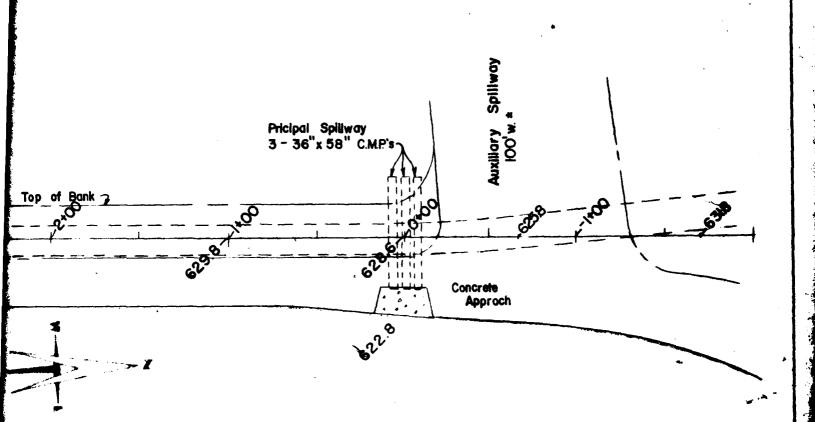
ent Drain

Top of Bank 7 Survey Base Line-Asphait) Drive Top of Bank

Water's Edge-

LAKE SHERWOOD Water Surface Elev. 622.0 (Aug. 25, 1978)

PLAN Scale: I"=50"

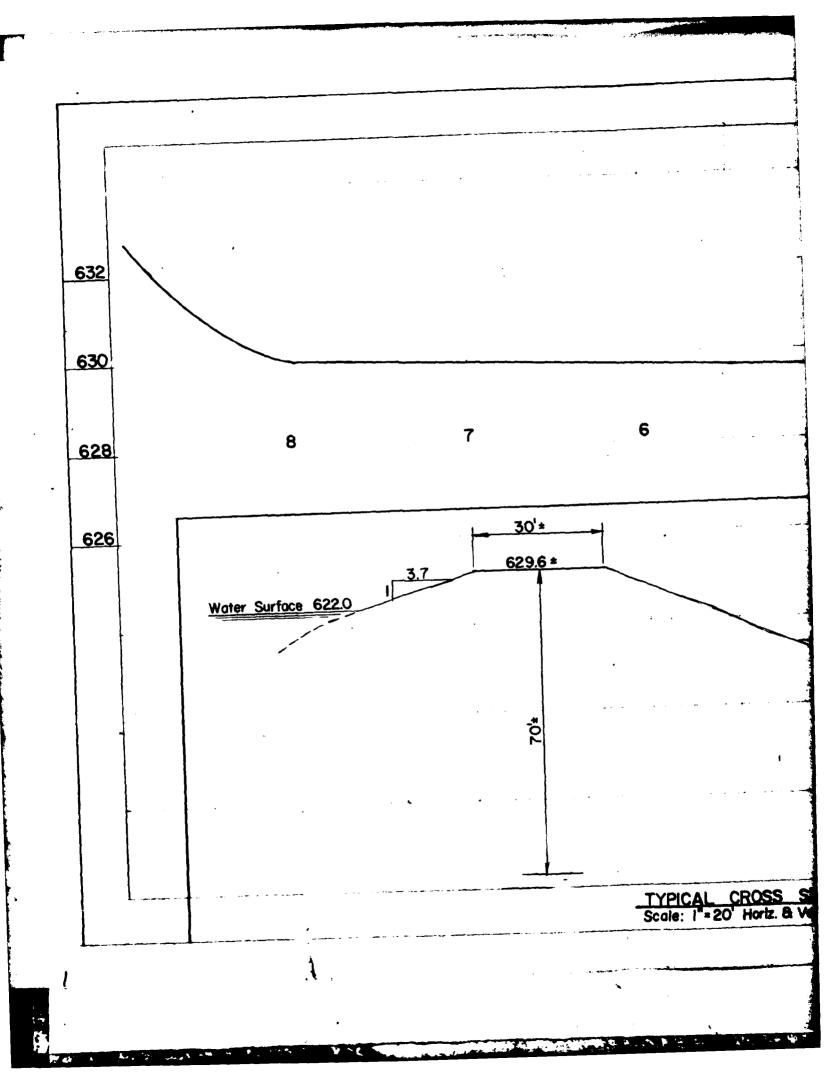


TOP OF DAM ELEVATIONS

Kenneth Balk & Asso. Inc.

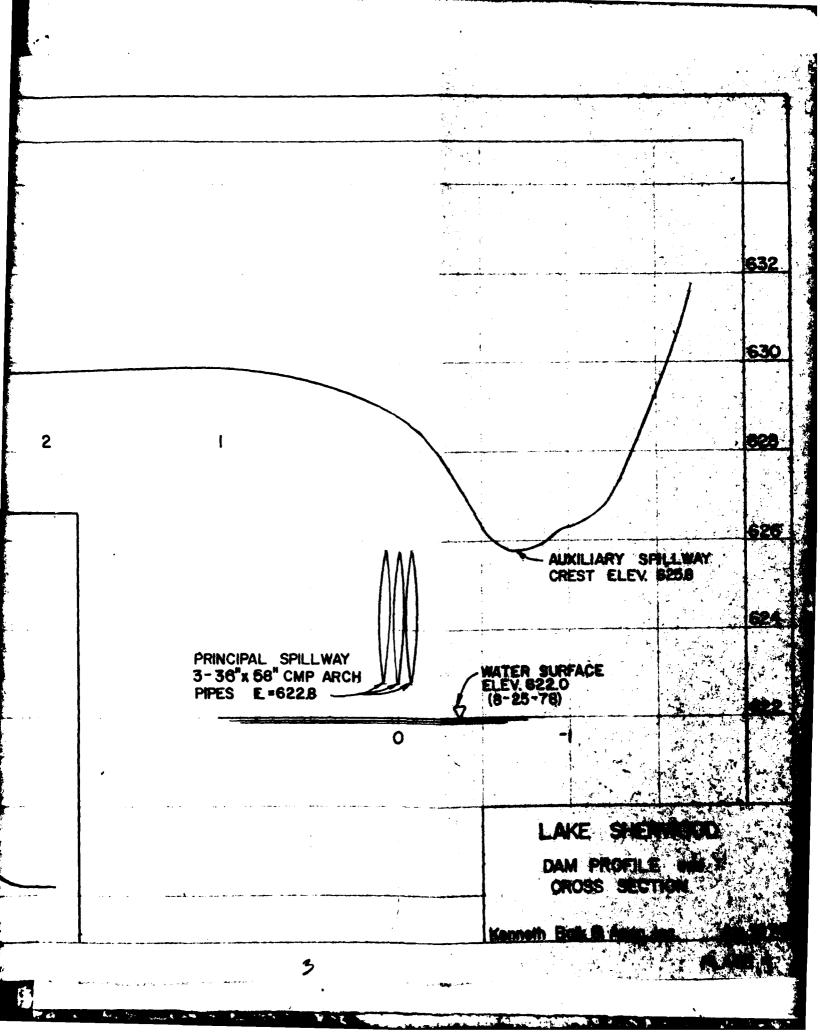
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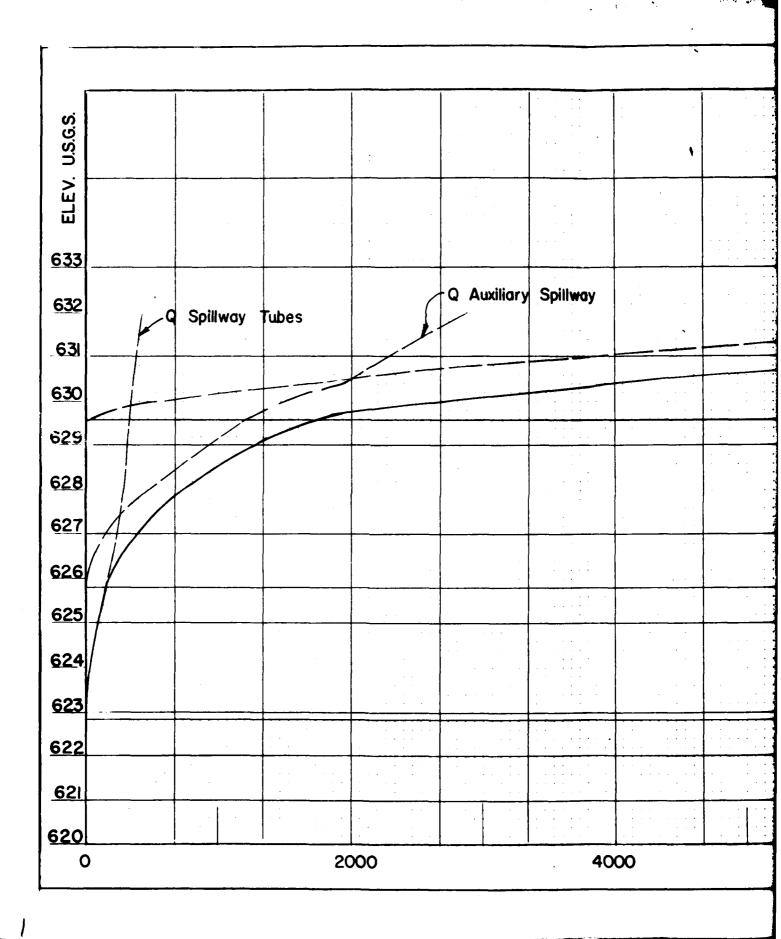
PLATE 3



TOP OF DAM 5 2 TOP OF DAM PROFILE
Scale: I"= 2' V., I"=50' H. PRINCIPAL 3-36"x 56" PIPES E

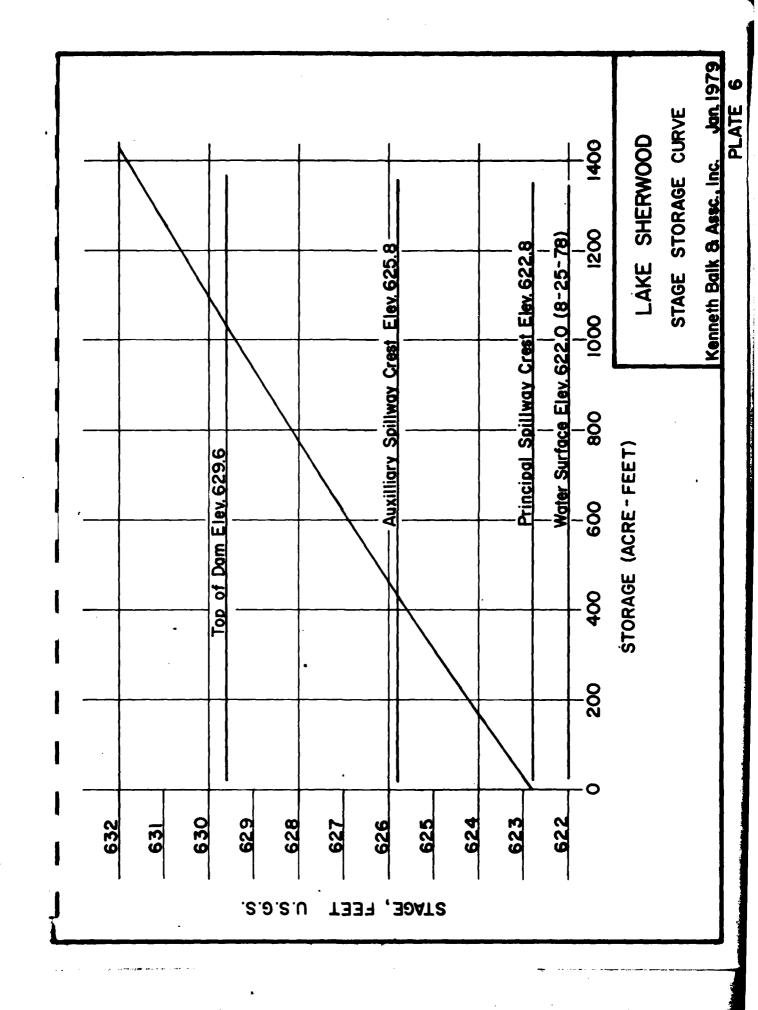
SECTION Vert.





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					Wate	Surface E	ev. 622.0	(8-25-78)		-
			1		Princ	ipal Spillwe	cy Crest E	ev. 622.8		-
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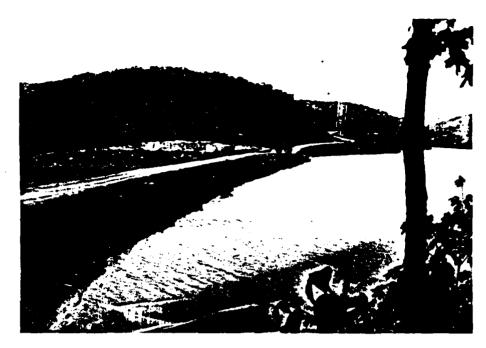


PHOTO I

Overview of Lake and Dam



PHOTO 2 View from North Bank of Principal Spillway Entrance



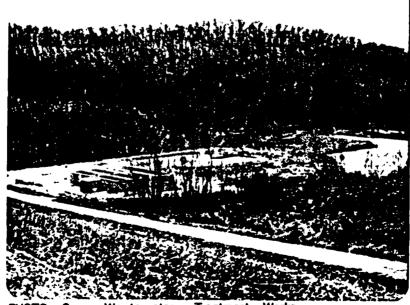
PHOTO 3 View from Top of Dam of Principal Spillway Entrance



PHOTO 4 Principal Spillway Exit



РНОТО 5 Spring in Left Abutment near Toe of Embankment



### APPENDIX A

HYDROLOGIC AND HYDRAULIC ANALYSIS METHODOLOGY

### HYDROLOGIC AND HYDRAULIC ANALYSIS METHODOLOGY

- The hydrologic analysis used in development of the overtopping potential is based on applying a hypothetical storm to a unit hydrograph to obtain the inflow hydrograph for a reservoir routing. The Probable Maximum Precipitation is derived and determined from regional charts prepared by the National Weather Service in "Hydrometeorological Report No. 33." Reduction factors have not been applied. A 24-hour storm duration is assumed with the total rainfall depth distributed over 6-hour periods in accordance with procedures outlined in EM 1110-2-1411 (SPF Determination). The maximum 6-hour rainfall period is then distributed to hourly increments by the same criteria. Within-the-hour distribution is based upon NOAA Technical Memorandum NWS HYDRO-35. The nonpeak 6-hour rainfall periods are distributed uniformly. All distributed values are arranged in a critical sequence by the SPF criteria. The final inflow hydrograph is produced by utilizing the Soil Conservation Service triangle unit hydrograph using Hydrologic Soils Groups "B" and "D". Antecedent Moisture Condition III, and SCS CN 82 used to determine rainfall excess.
- 2. The reservoir routing is accomplished by using Modified Puls routing techniques wherein the flood hydrograph is routed through lake storage. Hydraulic capacities of the outlet works, spillway, and crest of dam are used as outlet controls in the routing. Storage in the pool area is defined by an elevation-storage capacity curve. The hydraulic capacity of the outlet works, spillway, and top of dam are defined by elevation-discharge curves.
- 3. Dam overtopping analysis has been conducted by hydrologic methods for this dam and lake. This computation determines the percentage of the PMF hydrograph that the reservoir can contain without the dam being overtopped. An output summary in the hydrologic appendix displays this information as well as other characteristics of the simulated dam overtopping.
- 4. The above methodology has been accomplished for this report using the systemized computer program HEC-1 (Dam Safety Version), July 1978, prepared by the Hydrologic Engineering Center, U.S. Army Corps of Engineers, Davis, California. The numeric parameters estimated for this site are listed in the attached computer printout. Definitions of these variables are contained in the "User's Manual" for the computer program.
- 5. The inflow hydrograph was routed through the reservoir using HECl's Modified Puls option. Releases were calculated for: 1) the principal spillway and, 2) the flow over the top of the dam. These releases were then combined at each of their respective elevations.

Flow through the principal spillways, three 36"x58" corrugated metal arch pipes, approximately 63.2 feet in length was obtained as follows:

### For Part Full Flow:

Stage = E.G. 
$$+ h_e$$

Where Stage = Pool Elevation

E.G. = Energy Gradient Elevation in pipe = 
$$d_f + \frac{v^2}{2g}$$

$$h_e = \text{entrance loss} = k_e \frac{v^2}{2g}$$
, with

$$k_e = 0.5$$

$$d_f$$
 = depth of flow for a given discharge

$$\frac{V^2}{2g}$$
 = velocity head

The equation then reduces to:

Stage = IE + 
$$d_f$$
 + 1.5  $\frac{v^2}{2g}$ 

### For Full And More Than Full Flow:

Stage = IE + 
$$D_m + \frac{v^2}{2g} + h_f + h_e$$

Where Stage = Pool Elevation

$$D_m = Minor Axis of pipe = 3.0 feet$$

$$\frac{V^2}{2g}$$
 = Velocity head

$$h_f = Friction loss = \frac{Q^2}{K_C} \times L$$

Q = Discharge in cfs.

 $k_c$  = Conveyance coefficient = 634.93

L = Length = 63.2 feet

 $h_e = Entrance loss = k_e \frac{v^2}{2g}$ , with  $k_e = 0.5$ 

With proper substitution of numbers, the equation reduces to:

$$Q = (\frac{\text{Stage-625.32}}{.00034})^{\frac{1}{2}}$$
 South Tube

$$Q = \left(\frac{\text{Stage-625.02}}{.0034}\right)^{\frac{1}{2}} \text{ Center}$$

$$Q = \left(\frac{\text{Stage-624.71}}{.00034}\right)^{\frac{1}{2}}$$
 North Tube

Flow through the overflow spillway and over the top of dam was calculated using the weir flow equation:

$$Q = CL(H)^{1.5}$$

where: C = Varies with head as outlined in "Handbook of Hydraulics" by Horace Williams King, revised by Ernest F. Brater.

L = Length in feet (varies with water surface)

H = Head of water in feet (varies with water surface)

Q = Discharge in cfs

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LAKE SWERWOOD WULTI-PESRRVOIR ROUTING JAN, 1979 WO, INV, NO, 10202

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MULTI-PLAN ANALYSES TO BE PERFORMED NOLANE 1 NRTIDE 6 LATIOE 1 .00 07. RT105= \*\*\*\*\*\*\*\*\* \*\*\*\*\*\*\*\* \*\*\*\*\*\*\*

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72-HOUR 11. 2.30 54.43 58.43 20.30 20.30 58.43 20.43 6-HOUR 34. 1.88 47.75 17. 99. AT TIME 16.00 HOURS PEAK 99. CFS CMS TNCHES MA AC-FT THOUS CU M

MAXIMUM STORAGE =

707AL VOLUME 3027. 86. 26.43 58.43

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4:446677	6.664	699.A	699.A	699.8	8.654	699.B	6.669	4.99A
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	700.4	7007	7.007	7.007	7.007	7007	700.A	700.8
_	700.9	700.9	700.9	700.9	701.0	701.0	701.0	701.0
	761.1	701.1	791.1	701.2	701.2	791.3	701.3	701.4
_	701.6	701.7	701.8	701.9	701.4	702.0	702.1	107.1
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_	702.7	732.K	702.5	702.5	702.5	702.5	702.5	707.4
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-	102.1	792.1	702.1	702.1	702.1	702.0	702.0	702.0
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TOTAL VOLUME	202.	137.74	61.
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344. AT TIME 15.83 HOURS

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,	700.0	701.3	701.6	701.9	702.7	703.0	703.2	703.3	707.4	70.5	703.1	707.7	702.4	702.2	702.0	702.0	701.9	701.9
	700.9	701.2	701.6	701.8	702.5	703.0	703.2	703.2	703.5	7.03.2	703.1	102.7	702.4	702.2	702.1	702.0	701.0	701.9
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	700.8	701.1	701.5	701.9	702.4	702.9	101.1	703.2	7.64	707.	703.1	702.9	707.	702.2	702.1	702.0	792.0	701.9
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# STATION OUTING, PLAN 1. RATIO & END-OF-PERIOD HYDROGRAPH OPDINATES

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STATION DUTING. PLAN 1. RATIO 5 END-NF-PERIOD HYDROGHAPH OPDINATES

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STATION OUTING. PLAN 1. RATIO 6

# END-OF-PERIOD HYDROGRAPH ORDINATES

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<u> </u>	666 14 666 666 666 666 666 666 666 666 6	106.4

15.43 HOUPS
TIME
1802. AT
9
12
OUTFLOW
EAK

TOTAL VOLIJME	40974.	1160.	31.14	190.97	282.	348.
72-H0UR	142.	;	31.14	790.97	2A2.	74B.
24-HOUR	142.	÷	31.14	790.97	282.	346
6-HOUR	464.	13.	25.41	645.33	230.	. A4.
PEAK	1802.	51.				
	CFS	CMS	INCHES	1	AC-FT	THOUS CU M

### MAXIMUM STORAGE . 26.

SUB-AREA HUNDEF COMPUTATION

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SURARE: RUNDEF FOR LAKE MARIAN ISTAGE TAUTO ISTAGE TAUTO INFLOW 0 -0 -0 1 3 1 -0 -0 -0

INTEG 10HG TAKEA SAND INSUE WATTO ISNOW ISNUE LOCAL  SPFF PMS RS R12 R24 R48 R77 R96  -0.00 26.00 100.00 120.00 -0.00 -0.00 -0.00  LOSS DATA  LOSS DATA  CORVE HO -0.00 1.00 -0.00 -1.00 -1.00 -0.00  CORVE HO = -82.00 WETNESS = -1.00 EFFECT CN = 82.00	2 2					4000				
SPFF PMS R\$ R12 R24 R48 R72 R96 -0.00 2A.00 100.00 12A.00 130.00 -0.00 -0.00 -0.55 DATA STRKP DLTKR RTIOL EPAIN STPK RTOK STRTL CNSTL 4LSWX -0.00 -0.00 1.00 -0.00 -0.00 -0.00			0.00	.04	1.00	-0.000				٩
-0.00 26.00 100.00 120.00 130.00 -0.00 -0.00 -0.00  LOSS DATA  STOKE PLIKE RIJOL ERAIN STOKE RIJOK STRTL CNSTL ALSWX -0.00 -0.00 1.00 -0.00 -0.00 -0.00  FROM -82.00 WETNESS = -1.00 EFFECT CN = 82.00		ž. Vi	Š	PRECIP	DATA R24	8. 8.			96	
LOSS DATA STRKP DLTKR RTIOL EPAIN STRKS RTIOK STRTL CNSTL ALSWX -0.00 -0.00 1.00 -0.00 -0.00 1.00 -1.00 -82.00 -0.00 IF HO # -82.00 WETNESS = -1.00 EFFECT CN = 82.00		00 100	. 00	20.00	130.00	-0.00			00	
	2	9	9	1055 1	)ATA	. 5		T SA	2	
WETNESS = -1.00 EFFECT CN =	-0.00	1.00	10.0	0 0		00	180	2.00	-0.00	
	-82.00	WETNES	II	-1.00	FFECT C		00-21			
		5LTKR -0.00 -82.00	10.TKA RTIOL -0.00 1.00 -82.00 WEINES	RTIOL 1.00 WETNES	RTIOL 1.00 WETNES	RTIOL 1.00 WETNES	LOSS DATA PTIOL EPAIN STEKS RTICK 1.00 -0.00 -0.00 1.00 WETNESS -1.00 EFFECT CN UNIT HYDENGRAPH DATA TC=-0.00 LAS= .20	LOSS NATA PTIOL ERAIN STRKS RTIOK STRL  1.00 -0.00 -1.00 -1.00  WETNESS = -1.00 EFFECT CN = 82.00  UNIT HYDPOGRAPH DATA  TC = -0.00 LAG -20	LOSS NATA 10L ERAIN STRKS RTICK STRL 1.00 -0.00 -0.00 -1.00 WETNESS = -1.00 EFFECT CN = 82.00 UNIT HYDDAGRAPH DATA TC= -0.00 LAG= .20	LOSS DATA RIOL ERAIN STRKS HTICK STRTL CNSTL 1.00 -0.00 -0.00 -1.00 -82.00 WETNESS = -1.00 EFFECT CN = 82.00 UNIT HYDPOGRAPH DATA TC= -0.00 LAG= .20

UNIT HYDROGRAPH 14 END OF PERIOD ORDINATES, TC= -0.00 HOURS, LAG\* .20 VOL\* 1.00 28. 93, 116. 97, 51, 51, 30, 17, 10. 5. 2. 1. 1. 0. HECESSION DATA STRIGE

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	Z Y	12.05	12.10	12,15	12.20	12,25	12,30	12,35	12.40	12,45	12,50	12.55	13.00	13,05	13,10	13,15	13.20	13,25	13,30	13,35	13.40	13.45	13,50	13.55	14.00	14.15	14.10	14.15	14.70	14.25	14.30	14,35	14.40	14.45	14.50	14.55	15.00
ũ	40.C	1.01	1.91	1.01	1.01	10.1	1.01	1.01	1.01	1.01	1.01	1.01	1.01	10.1	10.1	1.01	10.1	1.01	10.1	1.01	1.91	10.1	10.1	10.1	10.1	1.01	1.91	10.1	10.1	10.1	100	1.03	1.01	1.1	1.01	1.61	
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0	40.0x	1.01	1.1	1.91	1	10.1	1.01	1,01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	1.01	10.1	1.01	1,01	1.01	10.1	1.01	10.1	1.01	1.e	1.01	1.01	۲. د	10.1	1.01	1.01	1.31	1.01	1.01	٦.٠	1.,1	3

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HYDROGHAPH AT STAINFLOW FOR PLAN 1. PTIO 1

TOTAL VOLUME 1443. 41. 3.21 24-HOUR 5. 6-HOUR 16. 7.54 64.42 CFS CMA TWCHFA

10.	2 TOTAL VALUME 24.3 6.43 164.3 26. 25.	3 TOTAL VOLUME 4329. 123. 9.64 244.95 30.	101AL VOLUPE 5772- 163- 163- 163- 325-60 49-	7 07 AL VOLUME 7215. 204. 16.07 40.4.25 50. 61.	10 6 TOTAL VOLUME 14431. 30.15 915.50 123.
10.	PLAN 1. RT10 72-HOUS T 10. 6.43 153.30 75.	PLAN 1. ATIO 72-HOUR T 15. 0. 9.64 2.445 30. 47.	72-HOUR 72-HOUR 10. 12. 16. 326.56. 40. 49.	72-HOUR 75. 15. 07. 16.07 4.08.25 60. 61.	72-HOUH 72-HOUH 50. 32-15 816.50 99.
10.	FOR 40UR 10. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	AINFLOM FOR PI R 24-HOUH 15. 0. 17. 244.95	AINFLOW FOR P  R	AINFLOW FOR F 24-HOUR 25- 11- 16-07 408-25 61-	STAINFLOW FOR INIUS PA-HOUP 50. 35.34 32.15. 32.15. 25 815.50 778. 123.
	6-HP18 24-1 32-32-32-15-17-17-18-15-15-15-15-15-15-15-15-15-15-15-15-15-	AT ST 6-HOU 47 47 193.2	63 63 10-1 757-7	6-HOU 79 70 12-5 322-1	A 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
:	НУОЯОСФАРН РЕА< 131. 4.	нү <u>э</u> кобаарн Релк 147. 6.	итляпачарн релт 263. 7.	нүовобкарн Реак 328. 9.	нувареварн РГак 657. 19.
AC-FT THOUS CU M	CFS CMS CMS INCHES AC-FT THOUS CU M	CFS CMS FNCHES MM AC-FT THOUS CU M	CFS CHS TNCHES TH AC-FT	CFS CWS TWCHES AMA AC-FT	CFS CMS TNCHES WW MC-FT

763.	15.27	347.92	186.	729.
	15.27	397,92	185.	.666
e,	15.27	387.92	146.	229.
34.	12.61	320.24	153.	180.
	INCHES	Z	AC-F?	THOUSE CO #

	•	VOLUME	55405.	1569.	31.40	797.45	382.	471.
	4110 6	TOTAL				٠		
•	PLAN 1 NTIO 6	72-HUUR	192.	S	31.40	797.46	382.	471.
:	AT	H101-40	192.	5,	37.49	797.46	382,	471.
•	SUM OF 2 HYDROGRAPHS AT	R-HOUR	622.	<u>.</u>	25,38	644.55	308.	384.
	OF 2 HYD	PFAX	2391.	64.				
	MAS		CFS	520	SHUNI	<b>314.</b>	AC-FT	THUNG CO 34

					675.5	.14.										
					675.0	.7.	•	675.					•	• • •	9.	
*****		18610			674.5	75.	35.	675.					•	••	• •	
•		ISTAGE -0	LSTR -0	ISPPAT -1	674.0 679.0	62. 7053.	31.	674.	ExpL -0.0					• •		
••••		INAME		STORA -571.			26. 76.	674.	CAREA -0.0		-	res	•	, .	56	
******		1447 B	dhdl -0	75K -0.00u	673.5 678.5	40. 5934.	21. 70.	673.	. 0.0-	DAMWIO -0-	. RATIO 1	H OPDINA	Ġ	• •	 	
•	UTING	196. 1	1061	¥ -0.000	673.0 678.0	27. 4861.	17. 65.	673. 678.	ELEVL -0.0	DAM DATA 100 EXPO	STATION OUTING, PLAN 1, RATIO 1	ENG-AF-PEP100 HYDROGRAPH OPPINATES		ċ	. c	
*******	HYDROGRAPH ROUTING	IECON ITAPE	ES ISAME	6 AMAKK 0 -0.900	672.5	16. 3702.			Expu	57	טא מעדנאפ	-PEP100 P	OUTFLOW	: 0	ė ė	
	HYOR	R LAKE F	2	L LAG		m	13.	672. 677.	\$000 -000	10PEL 574.8	STATE	END-UE	c	• •	• ·	
••••••		UTING FOR O ICOMP	5 AV6	S NSTOL	672.0	2550.	π.υ. • υ.	672. 677.	5P410				•		• •	
:		PESENVOIR ROUTING FOR LAKE MARIAN ISTAG ICOMP IS OUTING I	\$5 CLOSS	NSTPS	671.5 676.5	.5071	. ç	671. 675.	CREL 671.0				•			
:		R R	0*0- 55070		671.0	0. 556.	, 6 , 5	671. 676.					•		ee	
*****					STAGE 6	FLOW	CAPACITYE	ELFVAT I ON=					ě	•	<b>.</b>	

COMPINE HYDROGRAPHS

CFS 135. 48. 16.  CCS 4. 1. 96.  CCS 135. 1. 95. 54.34.  AC-FT 20. M. 22. MVOROGRAPHS AT  SUM OF 2 MYOROGRAPHS AT  10.03 12.04  AC-FT 15.0  10.03 12.04  AC-FT 15.0  SUM OF 2 MYOROGRAPHS AT  SUM OF 2 MYOROGRAPHS AT  10.03 12.04  AC-FT 15.0  10.03 12.04  AC-FT 15.0  10.03 12.04  AC-FT 15.0  SUM OF 2 MYOROGRAPHS AT  SUM OF 3 MYOROGRAPHS AT  SUM OF	CFS 135. 48. 16. 16. CWS 135. 1.95 24. 31. CWS 135. 1.95 24. 31. CWS 13. 1.95 24. 31. CWS 13. 1.95 24. 31. CWS 13. 13. 4.68 35. CWS 13. 4.68 115. 13. 4.68 35. CWS 13. 4.68 115. 13. 4.68 115. CWS 13. 4.68 115. 13. 4.68 115. CWS 10. F. AVOROGRAPHS AT SUM OF 2 HYDROGRAPHS AT 12.06 305. THE SUM OF 2 HYDROGRAPHS AT 12.06 305. THE SUM OF 2 HYDROGRAPHS AT 15.0 M	E	1 157 460	14070
CFS 135. 48. 16. 16. 16. 16. 16. 16. 16. 16. 16. 16	CFS 135. 48. 16. 16. 16. 16. 16. 16. 16. 16. 16. 16	1 RT10		
CFS 135. 48. 16. 16. 16. 16. 16. 16. 16. 16. 16. 16	CFS 135. 48. 16.  CMS 40.47 64.34  MAY 24.7 64.34  AC-FT 2 40.47 64.34  CU M OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  CC M M OF 2 HYDROGRAPHS AT  CC M M OF 3 HYDROGRAPHS AT  C	TOTAL	340	
CFS 40.25 2.53 2.53 6.34 6.34 6.34 6.34 6.34 6.34 6.34 6.3	CES 1.95 7.53  NOMES 40.47 64.34  ACLET 20. N. 31.  CUL N. SUM OF 2 WYOROGRAPHS AT  SUM OF 3 WYO			
CES	NCFF S       1.05	• •	53	
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SUM OF 2 HYDROGRAPHS AT  CFS	CFS 451. 115. 35.  CWS 13. 4.78 5.68  NCMS 13. 4.78 5.68  NCMS 5 13. 4.78 5.68  NCMS 13. 4.78 5.68  NCMS 7 10. 70. 181. 5.68  CCS 710. 181. 5.68  NCMES 20. 7.39 8.85  NCMES 187. 83 224.70  SUM OF 2 HYDROGRAPHS AT  SUM OF 2 HYDROGRAPHS AT  CCS 710. 111. 133.  CC M  SUM OF 2 HYDROGRAPHS AT  SUM OF 3 HYDROGRAPHS AT  SUM OF		38.	
SUM OF 2 HYDROGRAPHS AT  CFS	CFS	0110		
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AC-FT 67. 69. 77.  CU # AC-FT 70. 69. 69. 65.  CU # PEAK 4-HOUG 24-HOUP 72-HOUH TOTAL V  CFS 710. 181. 54. 2. 2.  CUS 20. 7.39 8.85 8.85  RAPES 187.43 224.70  AC-FT 10. 181. 133. 133.  CU # BEAK 6-HOUR 24-HOUR 72-HOUR TOTAL V  SUM DF 2 HYDROGRAPHS AT PLAN 1 RTIO 4  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5  SUM OF 2 HYDROGRAPHS AT PLAN 1 RTIO 5	AC-FT 57. 69.  CU K 710. 70. 85.  CFS 710. 181. 54.  CUS 70. 181. 54.  CUS 70. 181. 54.  CUS 70. 181. 18.  SUM DF 2 HYDROGRAPHS AT  SUM OF 3 HYDRO	144.65	0.4	
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F76.1	6.624	£72,3	4.614	672.5	612.5	472.6	672.6	672.7	672.7
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	e 1	97.	196.	96	84.	71.	62.	49	39	34.	30.	•	•	•	•	•	•	•	•	•	•		: -	: -		ď	• .	•		<b>.</b>		E i	21.	35.	35.	35.	33.		ė			- K	•		0.17	6-179	2.7.7	67.7	27.7	67.79	67.10	671.1	671.1	671.2	671.2	671.3	4.174	471.4	671.7	672.0	672.4	073.
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	• •			•	* *	77.	67.	55.	43.	.3k.	32.		ć	•	•	•	•	•	ċ	•	•	e e	-:	:	2.	ζ.			•		•	• • • • • • • • • • • • • • • • • • • •		֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	•	٠ د د د	•		25.			• * *		0 167	0.110	471.0	67.7	671.0	671.0	671.0	671.0	471.1	671.1	671.1	471.7	611.2	471.3	671.4	671.5	F		
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				,	•	• ·	•		÷.	٠/٢	ť.		ć			: .	• •	•	•	•	•	ď	<i>-</i> :	:	-	٠,	,	٠,	,	· .,	, =				ָ ֖֖֖֖֭֭֭֭֭֭֡֞֝֞		2	ž	, v,	24.	2.	: :		0.174	67.79	671.0	671.0	671.0	671.0	671.0	671.0	671.1	471.1	٨٢١٠١	671.2	5.17.5	671.3	•	7.11.7	472.2	27.0	

13.60

	;			A7A. A	674.9	675.0	675.0	675.0	675.0
674.2	4.4.4	6.176		476.0	675.0	675.0	675.0		9.5.0
675.0	475.0	675.0	6.674	0.00	6.75.0	6.75.0	675.0	675.0	F. 4. 5
6.75.0	475.0	675.0	6/5.¢	0.0		6.474	474.7	674.7	674.0
6-7/9	474.0	6.414	674.A	***	4.474	4.4.4	4.4.4	674.3	674.3
674.6	474.6	674.5	674.5	6.4.7	474.1	674.0	674.0	674.0	673.4
674.3	674.2	674.2	5.4.6	100	6.73.A	673.7	673.7	473.7	673.0
673.9	473.9	673.R	573.H	67.5	673.5	673.5	673.5	673.5	613.4
673.6	473.6	673.6	673.5	6 674	673.3	6.13.3	673.3	613.3	473.3
471.4	4.5.4	473.4	27.50	6773	677	673.1	473.1		
113.	6.574	473.2	\ .						
FAK OUTFLOW IS	123. AT TIME	WF 16.75	HOURS						

**V** 30

TOTAL VALUME 7430. 210. 4.21 105.94 51.
72-HOUR 76. 11. 4.21 106.94 53.
24-HOUR 26. 1. 4.21 106.94 51.
6-HOUR 82. 3.34 84.44 61.
рлак 123. 3.
CFS CAS TACASS NA AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACASS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACA AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS AACAS

36. MAXIMUM STORAGE =

END-OF-PERIOD HYDPOGRAPH ORDINATES STATION DUTING. PLAN 1. RATIO 3

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•	;;		• •	<b>,</b>	•	•		-	-			; ,		::	27.	57.	235.	228.	152.	117.	90.	:	, <del>9</del>	,		, ,	37.		
		• •	•	••	•	•	<b>.</b>		•	: ,	• •	•	;	10.	25.	53.	90.	251.	157.	124.	92.	76.	; ;	• •	• r. •	;	37.	33.	2
	• •	• •	;	•	•	<b>.</b>	<b>.</b>		• .	<b>:</b>	•	•	÷	٠,	23.	•	26.	281.	162.	128.		77.	- :		·	ţ	96	33.	
	••	c o	•	<b>.</b>	•	<b>.</b>	· .	<u>.</u>		•	٠,	۶.	,	. 80		¥			7.7			,		, H.		ę,	3.B.		:
MO 13110				· c	•	ċ	ċ	<b>:</b>	<b>:</b>	<b>:</b>	~	2.	i <b>.</b>		•	· :	: •		•	•	131.	45.		£4.	59.		, a		• • • •
	•		• c			•	ċ	-:	-:	•			; ,		ì	£ ;	ž,	• • •		175.	133.	96.	82.	74.	<b>6</b>	4		,	•
	•		ċ	• •	•		•	-	-	: -	-	: ,	: ,	• ,	ė	16.	36.	. 29	501.	180.	136.		**	7	42		• •	• 5 E	52.
	ċ	• •	ė	• •	•	•			: -	: -	: ,	:,	•	m.	÷		33.	45.	542	190	139.	97.	ď		: 3		e v	.04	35.
	ċ	• •	÷	•	•	:	• •			<b>:</b> .	<u>:</u> .	-	2.	æ.	ۍ.	13.	31.	. F.	533.	194	163.	101			•	•	52.	•;	15.

	ċ	•	ċ	0	Ġ		Ċ	• <u>-</u>	-	-	: ,	•	•	•	, ,	ė	-	18.	<b>\$</b>	<b>*</b> ` <b>*</b>	37.	34.	35.	7	e e					•02													671.2				_			674.0			-					_		673.4	
•	•		•	0			ė		: -:	-	• •	<b>.</b> .	• •	•	ń	• :	0.	17.	52.	37.	37.	36.	36.	*	E	27.	. ,		• • • •	•																				673.9											
٠	•		•	0			ć	•			: .	; ,	, ,	•	, ,	ė	01	.9.	24.	34.	37.	36.	36.	96	~		ָ פֿער	Ċ	•	.12	19.		47.0	27.7	77.0	0.1.6		0.1.6	0.170	6/1.0	1.1.1	671.1	671.2	7.170	7.7.7	7 1.2	A71.7	672.2	672.9	673.8	674.A	675.2	675.1	675.0	6.474	674.5	474.2	673.B	673.6	673.4	673.2
	:	•	;	•	•				: -	: -		• ~	•	•		<b>.</b>	•	. 9	23.	33.	38.	36.	36.	34.	31.	3	2 0	• • • •	• • • •	· .	19.		471.0	2.1.0	27.	200		0.1.0	0	0	1.1.1	671.1	671.2	2.1.5	2110	47.7	671.7	472.1	6.72.8	673.1	674.6	675.2	475.1	675.0	474.9	674.6	5.419	413.9	673.0	440.4	673.3
	0	0	0	0	0	0	•		• -		- ?	4 "	٠. ٦	٠.	* 4	ه م		5		Ê	38		36		5									0 1 1 0	671.0			0.170	0.170	971.0	671.0	671.1	671.2	2.1.0	2.1.0		671.7	672.6	672.4	673.6	674.4	675.3	675.1	675.0	614.9	674.6	674.2	673.9	673.6	673.4	674.3
STORAGE	•		ċ	ė					-	• -	: ,	٠,	: ,	•	<b>;</b> ,	ė		7.	22.	29.	36.	36.	35.	35.					• 6		20.	STAGE		77.0		2.7.	0.1.0	0.1.0	0.1.0	0.1.0	0.1.0	671.1	671.2	2.1.0	67.63		2 1 2 9	672.0	672.7	673.5	674.3	675.4	675.1	675.0	6.4.9	674.6	674.3	673.9	673.7	673.5	673.3
	•	•	•	•				ė		•	• •	• •	• •	• •	<b>.</b>	ŗ,	æ	13.	23.	٠ ٣	•0•	36.	36.	· 5	35,		• • •	ָ נ	5.5	· 1 ·	20.		7 127	2.5	671.0		0.1.6	0.170	0 1 / 1	671.0	671.0	571.1	671.1	2.1.0	6.1.5	47.7	7.174	671.0	672.6	673.4	674.3	675.5	675.1	6.75.0	675.0	574.7	674.3	67.0	673.7	673.5	673.3
	•	•	•	ė	6					: -	• •	: .	• •	•	• 1	ָר י	٠,	13.	20.	28.	*0*	34.	34.	£.			• • • •	ė	રં ર	.1.	۶¢.		6 174	0.1.0	0.174	2.7.0	5116	0.1.6	0.74	0.179	671.0	671.1	671.1	2110	5.1.6	67.5	67.174	A7.	672.5	673,3	674.2	675.5	475.1	675.1	675.0	574.7	674.3	674.0	613.7	673.5	673.3
			•	ċ	ć	· c	· -	ċ		• -	- 1		٠,	<b>:</b> .	• 1	ŕ		12.	6	27.	<b>4</b> 1.	34.	42	, <u>.</u>					•	:	٠,		7	27.7			= -	2		v . I . v	6.11.0	471.1	671.1	2114	6,110		671.6	6.17.4	472.4	673.3	674.1	675.6	675.1	675.1	475.0	674.7	674.4	474.0	613.7	673.5	673.3
	•	ċ	ċ	•	0		<u>ئ</u> ے:		; ~	• -	• ,	: ^	• •	•	• .	ř	•		• ~	ş		17.	£.		-	,		•		· ·	• v v		7 167	22.0	27.7	23.00		0.1.0	0 - 1 - 0	671.0	671.0	671.1	671.1	2.1.6	2.1.0	471.5	47.74	671.8	672.4	673.2	674.0	675.6	675.1	675.1	675.0	674.8	674.4	674.1	673.8	673.5	673.3

TOTAL						109.
72-HOUR	45.	-	7.30	145,36	я9.	109.
24-HOUR	45.	-:	7.30	185.36	.68	109.
6-H0UR	145.	;	5.43	150.64	72.	99.
PFAK	545.	15.				
	CFS	CHS	TACHES	¥.	AC-FT	THOUS CO M

MAXIMIM STOPAGE = 41

STATION OUTING, PLAN 1, RATIO 4
END-OF-PERIOD HYDROGRAPH ORDINATES

	•	ć	÷	· -		-			: -	:	<u>:</u> .	:	ζ.	4	ţ	11.	27.	, ,	. 0	•		264.	195.	144.	00	77.	67.	57.	<b>4</b> 6.	39.			ć				ć			: -	•		ċ	•		
	•	•	•	· -			. 0		: _:	: -	: -	•	~•	۳,	'n	10.	2.	3		•	663.	267.	205	156.	93.	78.	68,	59.	47.	39.			0	0			ò		c	-	• -	:.	• •	•	÷	š
	•	•	•								: -	• ,	~	3,	'n.	6	27.			. 63	*20°	317.	208.	164.	90	90.	69	60.	48.	•0•	35.		ė		d		6		ć	• -	: -	- •	:.	• •	•	5.
	•	•	•	ċ	•		• 5			: -		•	۶.	<b>ب</b>	.5	<b>3</b> 0	ί.	, er	4			362.	214.	171	95.	82.	70.	61.	.64	•0•	36.		•	•	•	•	•			: -	-		; -	<b>.</b>	•	•
-			•	ć	0		•			-	:	• .		°.	'n	٠.	19.	<b>4</b> 6.	a			121	219.	173.	96.	A.	71.	62.	50.	<b>*</b> ]•	<b>-9</b> E						ė	· c	, ,		•	:,		• ·	<b>:</b> .	;
00,75,0		ċ	ċ	· -	•			: :		: -	• .	•	ζ.	3.	ທໍ	7.	17.	2	2	• • • •		700	223.	175.	97.	RS.	72.	<b>63</b>	52.	<b>*</b> 2•	36.	STOPAGE	0	•				ć			• •	<b>:</b> ,	i r	: .	'n	,
	0	ċ		· c		c					: -	•	<b>5</b>	3,	÷	7.	16.	e e		•		603.	227.	176.	100	P. A.	72.	64.	53.	47.	37.		0	ć			ć	· •	ć			<u>:</u> ,	: .	٠,	<b>.</b> *,	\$
	•	•	e	6	•	0			ć	-	• ~	•	۶.	٠,	*	٠,	14.	35,	70		. 74.	700.	233.	161.	308.	£ z	73.	65.	54.	44.	37.		ċ	0	c	6	•	6		· -	• •	: .	<u>.</u> ,	; ,	<b>.</b>	•
	•	ċ	ć	ć	c	· c		· -	, <sub>c</sub> '	· _	<b>:</b> _	<i>:</i> .	•	٨.	;	·,	13.	-	¥7	•		7.87	240.	185.	11.		٦4.	<b>, , ,</b>	55.	44.	34.		ć	É	` e			· -				÷.		٠,	e.	
	•	ċ	ċ	ć	·-	ċ	c			-	• _	•	:	٠,	;	<b>.</b>	12.		. Y		• • • •		251.	190.	131.	91.	75.	67.	54.	45.	39.		¢	<b>.</b>	•	-	ě			· e		• -	- (	• •	ř.	•

		9/3°3	673.3	673.4	6/3.4	673.4 10UPS		673.4 615. AT TIME	673.4 PEAK OUTFLOW IS
673.5	673.5	673.7	673.1	673.7 673.5	673.8	673.9 673.4	673.9	673.4 673.6	673.9
473.9	673.9	674.0	674.0	674.0	674.1	474.1	674.1	674.1	K76.2
674.2	674.2	674.3	674.3	674.3	674.4	4.414	674.4	474.5	67~.5
674.5	674.6	674.6	474.7	674.7	674.7	674.A	67.B	674.3	614.9
674.9	6.479	674.9	675.0	675.0	675.0	675.0	47:41 0.574	1.57.4	0.076
675.1	675.1	675.1	5.579	675.2	675.2	675.2	675.2	675.2	675.2
675.7	675.3	675.3	675.4	675.4	675.5	1.5.1	47.5.A	474.9	6.5.29
674.9	17.47	475.5	675.3	675.2	615.2	675.1	475.1	475.1	1.529
675.0	614.9	674.8	674.7	674.6	674.5	4.414	674.3	674.2	674.1
674.0	613.9	673.8	473.7	673.6	673.5	673.4	673.3	473.2	1.179
673.0	612.9	672.8	672.1	1.619	677.6	677.5	477.4	612.3	672,3
672.2	672.1	472.1	472.1	672.1	672.0	672.0	671.9	471.9	471.9
671.9	671.8	671.A	671.4	6.11.9	671.H	671.7	671.7	7-125	r
67.17	6110	671.5	9.174	671.6	4.1.4	4.1.4	4.1.4	41.6	4.170
671.4	671.3	671.3	671.3	671.3	671,3	671.3	671.3	571.3	671.3
671.2	5.179	671.2	671.2	511.2	671.2	471.2	671.2	5.174	671.2
671.2	671.1	671.1	671.1	671.1	671.1	671.1	671.1	671.1	671.1
671.1	671.1	671.1	671.1	671.1	2.1.0	67.179	67.79	671.0	0.174
671.0	671.0	671.0	671.0	671.0	671.0	671.0	673.0	671.0	671.0
671.0	671.0	671.0	671.0	671.0	671.0	671.0	671.0	471.0	A71.0
671.0	671.0	671.0	671.0	671.0	671.0	671.0	671.0	671.0	671.0
671.0	671.0	671.0	671.0	671.0	671.0	671.0	471.0	6.17.	6.11.0
671.0	671.0	671.0	671.0	671.0	671.0	671.0	671.0	671.9	671.0
ļ	,	1	į		STAGE				
		-02	20.	02	٠٥٠	20.	Ξ.	21.	21.
21.	21.	21.	22.	22	ζ.	22.	200	٠,	23.
23.	23.	23.	23.		. 40	. 4	,		. sc
 	52	· ·	50.	. 40	. 4				T. C.
	ž.			20.	, , ,	, , ,	ָרָרָ בְּיִרָּ בַּיִּרְיִבְּיִרָּ		
	• •	ָרָ צְ	, c	• •	Ţ. S	֓֞֝֞֜֜֝֞֜֝֓֓֓֓֓֞֝֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓֓֓֓֓֡֓֓֓֡֓֡֓֡֓֓֡֓֡֓֡֡֡֡	ć t		
36.	36.	36.	96.	36.	36.	M	36.	34.	37.
37.	37.	37.	37.	37.	37.	37.	37.	37.	37.
37.	38.	38.	39.	•0•	÷:	42.	43.	**	**
**	42	• 0 \$	38.	37.	37.	37.	37.	¥.	36.
35.	34.	34.	33.	32.	31.	ě	29.	π. . λ.	. 1.2
	52.	***	24.	73.		21.		- 6	• • •
•		• •	* 4	•	ď	œ ç	œ ;	œ ;	• ;
-	•		٠,	÷	•	ç	•	ć.	÷

TOTAL VOLUME 18393. 521. 10.42 264.74 127. 156.

72-40UR 64. 2. 10.42 264.74 127. 156.

24-HOUR 2. 10.42 264.74 127. 156.

6-HOUR 211. 3.60 218.45 105.

> CFS C4S C4S C4S AM AC-FT THOUS CU 4

PEAK 815. 23.

STATION OUTING. PLAN 1. RATIO 5

END-OF-PERIOD HYDROGRAPH ORDINATES

	•		ć		; c	· e		: -		- 6	•	•	ė		21.	51.	• u6	279.	1644.	319.	242.	179.	95.	œ.	.69	6.	0.50	47.		,	<b>.</b>	•	•	•	• •	•	<u>:</u> -	: ~	,,,			•	::	15.	<b>5</b> 4.	34.	34.	45.	39.	37.	34.	35.	'n		
	•	6		•		6			-	• •	in	•, •,	<b>.</b>		. 61	• • •	.95	275.	794.	347.	250.	195.	96	R2.	70.	62.	51.	43.		•	<b>.</b>	•	<b>.</b>	•	•	•	• -	: -		*	s.	7.	10.	 	23.	33.	38.	*	39.	37.	37.		36.		
				ć	ć		ċ	<b>.</b>	-	• •	• .	•	ė	10.	19.	7	61.	270.	581.	3AA.	257.	207.	96	933	71.	6.9	5.5	43.	38.	•	ċ	•	•	•	•	•	<b>:</b> -	-		; ;	ŝ	7.	10.	13.	22.	32.	38.	-	39.	37.	37.	35.	N O	. 4	
	•	0	•	•		•						•๋ เ	ń	• •	16.	38.	76.	262.	417.	446.	263.	214.	97.	85.	72.	ě	53.	•	38.	•	•	•	•		•	•	• -	: _		, M	s.	7.	10.	13.	21.	31.	37.	36.	40.	37.	37.	32.	, , ,		
					ć			; ~	: -	• •	• •	ຳ (	<b>.</b>	•		35.	73.	751.	330.	555	264.	216.	100.	. B	73.	· ·	7,	45	39.		•	<b>.</b>	• •	•	• •	• •	• -	: _:		ď	Š	7.	•	12.	<b>50</b>	30.	37.	38.	-	37.	37.	35.		30.	:
30 15110						Ċ		• -	: .	<u>.</u> .	<u>.</u> .		ı.	•	15.	32.	70.	236.	292	615.	271.	219.	100	9.8	74.	. 44	3,4	* 2	39.	STORAGE	ċ	•	•	•	• •	÷ •		• _				•	6	12.	19.	<b>5</b> 6.	37.	38.	42.	39.	37.	÷.	E	30.	•
	•				ć			• -	: .	• .	<b>∴</b> ,		·°	æ.	14.	29.	67.	215.	. 77.	714.	27%.	222.	136.	90	7	, v	57.		39.		<b>.</b>	•	•	•	ċ	• •	<u>.</u> -				•	ç	•	12.	1 H.	A.	37.	38.	43.	38.	37.	34.	•	. ac	•
	•		• •						•	<b>:</b> ,	<u>.</u> ,	Λ.	•		13.	27.	64.	141.	275.	819.	279.	225	133.		74.	, 1,	53.	47.	•0•		•	c ·	•	• •	• •	ř	• •	-		ئم :		•	æ	::	17.	27.	34.	34.	;	38.	37.	36.	***	31. 4	•
	ë					•		• •	• -	<u>:</u> ,	<b>.</b> .		•	7.	٦.	٠,٧	۶.	124.	274.	942.	2 P B .	23n.	147	95	77.	. 64	7		· c			ė	<b>.</b>	•		• •		• -	: ^			٠,	ď	::	7.	۶,	34.	38.	<b>*</b> ¥	34.	37.	¥. i	• F. 6	31.	: !
	ċ								: -	• .	<u>.</u>	:	•		۲.	22.	54.	95.	2.H.C.	1041	3ng.	234.	[6]	*	2	6.6	\$	3,	÷		<b>.</b>	ė,	• e	•	• •	•	•	-		,	;	ţ			15.	. 25.	35.	34.	<b>,</b> 6.	36.	٠/٤			3.0	

25.	m n	23,	23.	23.	23.	22.		22.	25.
•	•	•	•	STAGE		;	;		
0.1	671.9	471.4		671.0	•	671.0	671.0	671.0	671.0
٠.	471.0	471.0		671.0	v	671.0	671.0	671.0	671.0
1.0	471.0	671.0		671.0	•	671.0	671.0	671.0	671.0
1.0	671.0	571.0		671.0	v	671.0	671.0	671.0	671.0
٠.	671.0	671.0		671.0	•	671.0	671.9	671.0	671.0
٠.۶	471.0	671.0		671.0	•	671.0	671.0	671.0	671.0
571.0	471.9	671.1	671.1	671.1	671.1	671.1	671.1	671.1	671.1
7.7	571.1	671.1		671.1	£	671.1	671.1	671.1	471.1
-:	471.1	471.1		671.1	£	671.2	671.2	671.2	471.2
2.	471.2	671.2		671.3	9	671.3	671.3	571.3	671.3
1.3	671.3	471.4		671.4	v	471.4	671.4	671.5	671.5
۲.5	671.5	671.5		671.6	•	671.6	671.5	671.4	671.7
١.٦	471.7	671.7		671.9	Ψ	671.8	671.9	6.11.9	671.9
٠.	672.0	677.0		672.1	Œ	6.72.2	672.2	672.2	672.3
~.	6773.3	4.27.4		672.4	w	672.5	672.6	672.7	677.7
Ξ,	6.676	673.0		673,2	œ	673.4	673.5	673.6	673.8
٥.	676.1	674.1		674.3	v	674.5	674.6	674.7	674.8
6.	475.0	675.1		675.2	•	675.2	675.2	675.2	675.2
٠.	475.2	615.2		675.3	v	4.5.4	675.6	675.9	676.1
	474.1	6.029		675.7	•	675.5	675.4	675.3	675.3
· 3	674.3	474.2		675.2	w	675.2	675.2	675.2	475.2
	475.2	675.2		675.2	•	675.2	675.1	675.1	675.1
	475.1	6.75.0		675.0	•	675.0	675.0	675.0	6.474
6.	474.4	6.114		674.B	v	674.7	474.7	674.7	674.6
9	474.4	674.5		674.5	Œ,	674.4	4.419	674.3	674.3
6.1	474.2	674.2		574.1	·	674.1	674.0	674.0	674.0
0.1	673.9	613.9		613.9	•	673.B	673.A	673.A	473.7
۲.	K73.7	473.7		673.6	v	673.6	673.6	673.6	673.5
٠,	473.5	473.5		673.5	•	477.4	477.4		

HOURS	
15.92	
TIFE	
1091. AT	
SI #0	
SUTFLOW	
PEAK	

TOTAL VOLUME 23972.	2
72-HOUR 83.	13.58 345.03 165.
24-HOUR 83.	13.58 345.03 165.
6-H0UR 278.	11.35 288.24 134.
PEAK 1091.	• - -
2.5.5 2.5.5	TNCHES  AM  AC-FT  THOUS CU M

### MAXIMUM STORAGE # 46.

### STATION OUTING. PLAN 1. RATIO 6

## END-OF-PERIOD HYDROGRAPH OPDINATES

				OUTFLOW					
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:	e.			ċ		•	•	•	ċ
				•		<i>:</i>	<b>:</b>	<b>:</b>	<b>:</b>

2.		13.	2A.	47.	•69	· ·	340		2278.	616.	464.	328.	120.	• 00	78.	٠,	65.	.65			•	•	•			• ·	: -	:		• •	11.	17.	23.	27.	33.	o e			42.	*0	38.	34.		• • •	27.	, v.			671.0	671.0	671.0	671.0	671.1	671.1	671.1	5,11,2	671.4	01101
	•	12.	26.	;	•	• . • .	• o		1973	457	4.83.	370.	133.	92.	75.	71.	65.	.09			•	•	• •	; <	• -	•	-	: -		•	11.	17.	22.	27.	32.	• •	•	52	45.	40.	39.	36.	46.	300	27.		,		_	-	~	-	~	_	671.1			I
		:::	24.	42.	63.	76.	365	F 6 7 .	1412	711.	503	403.	147.	43.	8u	71.	66.	61.	54.		•	• •	• •		• •	<b>.</b> -	-	• ,-			10.	16.	25.	. Se.	31.	œ.	•	8	<b>M</b>	<b>*</b> 0 <b>*</b>	39.	36.	34.	35.	27.		24.		671.0	671.0	671.0	671.0	671.1	671.1	671.1	671.2	671.4	0110
	'n	6	23.		. 62.	73.	320.	, the transfer of the transfer		777	520.	* T *	163.	• • •	61.	72.	.99	62.	55.		c	•	• •		•	· -	: -		. ~	ŝ	÷	16.	21.	Se.	30.	6.	0	<b>4</b> 5	;	* I *	39.	36.	32.	200	• <del>•</del>	26.	25.		671.0	671.0	671.0	471.0	671.1	671.1	1.124	671.1	6714.5	,
		. 40	<u>.</u>	38.	, o.	71.	46.5	, , , , , , , , , , , , , , , , , , ,	26.0	9 48	573.	423	180	95	A3.	73.	67.	62.	, 56.	Į,	,	•	•	•	•	<b>.</b>	-	: -:	: <		6	15.	21.		÷.	z. m.		<b>4</b> 2.		4.1.	39.	36.	3.5°	• • •	• A C		<b>5</b> 2	•	_		_	-	-	_	671.1			5-1-0
-		1	. c.	36.	S.	70.	377	- - - - -		1019	541.	425	194.	94.	94	73.	64.	63.	56.	STOOP							4 -	-	: .:	4	6	7.	20.	, s,	29,	æ.	• •		• 6	.1.	39.	37.	35,	* 6			25.	STAG		671.0	671.0	671.0	671.1	671.1	671.1	671.1	6,176	
-				34.	56.	79	27.B.	434		1264.	547.	0.24	214.	96		74.	. F.G	63.	57.		•	•	•	•	• <		• -				Ť	74.	29.	S	.62	. A.		; ;	. 1 4	÷	. 64	37.	ů.	, u	• a	, ,	25.		671.0	671.0	671.0	671.0	471.1	471.1	671.1	47	971.1	[•1]c
-	ď		17.	33.	2.	٠ چ	251.	2 0		72.5	2,7	4	234	~	. 7	, ,	***	ċ	51.		•	•	ė	•		• -	• -	•			7	13.	19.	*.	24.	37.	• • •	•	6	-	.04	37.	£.	, , ,		27.	25.		_		-	_	-	_	671.1			_
		. v	. 5.	31.	۶1.	٨٢.	172	* C C	- 1 - 1	1944	244	4	244.	101	4	75.	54	, t. 4	5.4		•	• •	• c	: 6	• •	• -	: -	• -	- ^		,	- 2		٠,٠	• •	35.	?	1 4			.04	٠٢٤.		; ;		27.	, v.		671.0	671.0	671.0	671.0	471.1	471.1	671.1	-1.1.4	5716	
. <u>-</u>			•	24.	?	ř. ř.		• • • •		22.42	7 4 5	25.4	22.	,,,	7	17.	7		• 6.		•	• .	• •	• •	•	•	• -	•	• ດ	شم	;	12.	14.	23.	٠ ٣	35.	2 2	-	, E	* ~ *	<b>*</b> u*	¥.	٠ د :	•	90		×.		671.0			•	•		671.1	•	•	1

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672.3	673.0	673.7	674.1	674.8	675.4	675.5	675.6	676.8	675.7	675.5	£75.7	675.0	674.8	674.6	674.3	474.1	673.9	
672.3	673.0	673.6	674.1	674.7	675.4	675.5	675.6	676.7	675.7	675.5	475.4	675.0	674.9	674.6	6.479	674.1	674.0	
672.2	472.9	673.5	674.0	674.5	4.274	6.75.5	475.6	675.3	675.8	675.5	475.4	675.1	474.0	674.6	4.4.4	674.2	474.0	A73.B
672.1	672.8	673.5	674.0	674.4	6.15.3	675.5	475.0	676.0	6.519	675.6	4.519	675.1	6.719	674.7	4.4.9	674.2	674.0	4.F7A
672.1	672.8	673.4	674.0	4.4.9	675.3	675.5	6.514	475.7	6.416	675.6	4.579	675.1	674.9	674.7	4.4.4	574.2	674.0	673.9
672.0	672.7	673.4	673.9	674.3	675.3	475.5	674.4	4.519	676.1	4.514	675.4	675.1	675.0	674.7	674.4	674.2	674.0	677.0
671.9	677.6	673.3	613.9	674.3	575.1	47.24	4.1.4	575.A	676.2	4.579	4.5.4	675.2	675.A	674.7	674.5	674.2	674.0	677
671.9	672.6	673.2	673.A	474.2	475.2	475.4	612.5	4.014	4.424	4.5.4	4.579	475.2	475.0	A74.A	474.5	6.414	674.1	673.0
671.A	472.5	473.2	573.4	474.2	475.1	475.4	7.5.4	475.4	474.4	4.274	475.5	475.2	47E.0	474.0	674.5	674.3	474.]	477.6
571.8	677.4	673.1	473.7	674.2	474.4	47.14	د.۱۱۰	675.6	674.0	575.6	575.5	175.3	375.1	574.H	574.5	474.3	574.1	671.9

PEAK OUTFLOW IS 7278, AT TIME 15.93 HOURS

TOTAL VOLUME	51904.	1470.	29.41	747.07	357.	441.
72-H0U4	190.	ູ້	29.41	747.07	357.	441.
24-H0UR	180.	ທໍ	29.41	147.07	357.	441.
A-H0UR	617.	17.	25.16	639.01	306.	377.
PEAK	2278.	45.				
	CFS	CMS	TACHES	3	AC-FT	THOUS CO M

MAXIMUM STORAGE = 53.

COMPUTATION
RUNOFF
SUM-AREA HUNDEF

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	-	SURARFA	RUNDE	F F0	ons a	ARHO	רוסאו		ġ		***		;	,	
		INFLOW 0 -0 -0 -0	ISTAN NFLOW	<b>5</b>	a 0	IEC	Z 0		)   		JPKI INAME ISTAGE	INAME	ISI	9 GE	14010
ä	IHVNG		IUHG TARFA 2 1.51		. G-	<u>4</u>	DROGRI TRSDA 1.51	HYDROGRAPH DATA SWAP TRSDA TRSPC RATIO -0.00 1.51 1.00 -0.000	age e	000	1 SNON	22	ISNOW ISAME	LOCAL	ه بـ
		SPFE -0.00	P45	~ ~	90.00	21	PRECIF R12 0.00	PRECIP DATA R6 R12 R24 100.00 120.00 130.00		R48 -0.00	H72 -0.00	896 -0.00	96		
ROPT STRKR	9.0	ر ا و ا	2 PLTKH P	PT10	٠.	PAIN 0.0	L055	LOSS DATA PTIOL EPAIN STRKS PTIOK 1.00 -0.00 1.00	110%	STRTL -1.00	7 0 8 0	CNSTL -A2.00	ALSMX -0.00		RTIMP .10
3	RVF	CURVE NO = -82.00		VETN	ESS =	•	1.00	VETHESS = -1.00 FFFECT CV =	3	82.00	00				

UNIT HYDHOGRAPH DATA

RECESSION DATA
STRTO= 3.07 OMCSN= -.10 RTIOR= 3.00

;	エルマスじつなった ー ことつ	X	5	_	DAULNA IESO		*******	3	•		200	
	214. 579. 54.	<b>,</b>				1179. 235. 24.	1231. 183. 18.		• • •	1088. 118. 12.	951.	
?	PE-21013	ت ا م ت	EXCS	5507	END-OF-PERTOD COMP 0	FLOW	I I	PERION	7 Y Y Y	Excs	5507	COMP
ċu.	-	۲۰.	00.	.01	e e	1.01	12.05	145	.22	.20	.01	787.
_	م	.0.	00.	ē.	ຕໍ່	1.01	12.10	1+6	.22	• 20	10.	817.
5.5	m.	ē.	00.		m •	ē:	12.15	141	25.	920	5.6	875.
<b>.</b>	ď		•	-	řu		30 01					1116
	r						12.30	4	, ,			1277
ي م	( -			: =	• a		12.35	151		7.		1447
3	- c	: =	000	į -	· _	10.1	12.40	152		12.		1613.
<b>V</b>	·	ē.	00	6		10.1	12.45	153	25			1764.
50	10	Ξ.	00.	6	13.	1.01	12.50	154	25	.21		1897.
. 55	=	ī.	.00	.0	14.	10.1	12,55	155	.22	.21	٠.	2005
96.	2	٤.	00.	.01	14.	1.01	13.00	156	55.	٤.	.01	2049.
•	٤1	₹0.	00.	.03	15,	1.01	13,05	157	, 26	.25	.01	2159.
• •	<b>:</b>	٠.	00.	٠٥.	15.	1.01	13.10	154	26	• 25	٠ ،	2252
÷	٠. م	• 0 ]	00.	٥.	16.	1.01	13.15	159	.26	\$2	٠.	2284.
ç	<u>*</u>	.01	00.	10.	16.	1001	13.20	140	.26	• 55	٠,	2352
ž	17	٥.	00.		<u>.</u>	1.01	13,25	141	• 26	٤,	٥٠	2424.
65.	<b>e</b>	6	00.	6	. 16.	1.01	13,30	162	2.	ຮູ	.0.	2498.
÷.	<u>ه</u> .	6	00.		. 17.	1.1	13, 15	163	٠. د د د	52.	= :	25.70
ç :	ر د .		e •	: c	. :	10.	04.51	164	ę,	Ç,	ē.	75.47
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5.5	ξ				17.	1.01	13,55	167	2	5		2792
00	54		06.	.0	17.	1001	14.00	168	56	52.	.01	2826.
5	ť	<u>-</u>	00.	ē	17.	1.01	14.05	169	35	.32	60.	2857
.10	ξ.	Ξ.	00.	.0	17.	10.1	14.10	170	.32	.32	10.	2893.
2.15	27	~ •	00.	~ •	17.	1.01	14.15	171	.32	32	٠.	2939.
ŏ	<b>₹</b>	ē.	00.	٤.	17.	1.01	14.20	172	•35	.32	.01	3001.
. 25	62	٠.	00.	.0	17.	1.01	14,25	173	.32	• 32	٠٠.	3078.
20	36	ξ.	.00	Ξ.	17.	10.1	14.30	174	32	.32	. 41	3164.
ũ	E E	ē.	00.	٥.	17.	1.91	14,35	175	.32	.32	٦.	3252.
4	32	-	00.	ē:	17.	1.01	7.40	176	32	32		3336.
•	<b>5</b>			= :	• • •	[ · ·	1 4 4		25.	÷ :		3413
2 1	9 4		•	= =		100	74.00	1 2	2.0	25.		
1 8	9.6			-	. a		15.00	7 80	, ,			3576
30.6	3.6	ē.	00	: 5			15.05					3500
07.	æ	~	00.	0	19.	1.01	15.10	182	4	39		3613
3.15	ě	.01	00.	ē.	20.	1.01	15.15	183	•	39	.01	3623.
3.20	04	ē.	00.	÷.	21.	1.01	15.20	184	•59	• 59	٠.	3647
ž	7	.01	00.	=	23.	1.01	15.25		69.	.69	.01	3725
.30	4	.91	00.	-	5 <b>4</b> .	10.1	15,30		1.68	1.66	-05	3965
35	43	ξ.	00.	ξ.	<b>56.</b>	1.01	15,35		2.17	2.74	٥,٠	4518.
•	;		.00	٥.	27.	1.01	15.40		1.09	1.04	.01	5414.
3.45	45	ē.	.00	ē.	29.	1.01	15.45	- B	÷.	6	ç.	4637.
ŏ	<b>4</b>	ē:	00.	6	30.	1.01	15.50	067	.59	ę,	.0.	9071
3.55	4	ē :	6.	ē	32.	1.01	15.15	161	•	6F.	06.	9356
6.	a :	Ē.	00.	.0.	33.	1.01	16.00	192	9.	93	e •	10188.
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718.	721.	724.	727.	130	133,	136.		144	746	148	75.1	75.37	755	757	750	76.	762	764	166	767	769	72.	777		113	17.5	. 92							•				TAINFLO	- MO119						.8.		TAINFLO							.964
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HYDPOGRAPH AT STAINFLOW FOR PLAN 1. RTIO 3

TOTAL VOLUME	110212.	3121.	9.43	239.52	159.	936.
72-HOUR	343.	:	9.43	239.52	149.	936.
24-H0UR	343.	11.	64.6	239.52	159.	936.
4-HOUR	1216.	34.	1.49	190.24	603.	744.
PEAK	3156.	.68				
	CFS	Ç	INCHES	Ī	AC-FT	THUIS CO H

# HYDROGRAPH AT STAINFLOW FOR PLAN 1. RTIO 4

TOTAL VOLUME	146949.	4161.	12.57	319-36	1012.	1246.
72-HOUR	510.	<u>:</u>	12,57	319.36	1012.	1748.
24-40UR	510.	74.	12.57	319.36	1912.	1248.
6-HOUR	1621.	46.	66.6	253,65	304.	.166
PEAK	4208.	119.				
	CFS	CAS	SHUNI	He	AC-FT	THAIS CU M

## HYDROGRAPH AT STAINFLOW FOR PLAN 1. HTIO 5

TOTAL VOLUME 183686. 5201.	15.72 399.20 1265. 1560.
72-ноUR 638• 18•	15.72 399.20 1265. 1560.
24-40UR 638. 18.	15.72 399.20 1265. 1560.
6-HOUR 2026. 57.	12.48 317.06 1005. 1239.
PEAK 5251.	•
0 F S	INCHES AN AC-FT

# HYDROGHAPH AT STAINFLOW FOR PLAN 1. RTIO 6

TOTA	1276. 367372.					
24-HOUR	1276.	36.	31.43	194.40	2530.	3121.
6-H0'1R	4052	115.	24.97	634.12	2010-	2479.
PEAK	10521.	298				
	CFS	SNO	INCHES	W	AC-FT	THOUS CU M

#### HYDROGRAPH ROUTING

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JPRT	<b>-</b> 0	IPMP	î	1SK	-0.000
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SUGARHO	0 0	1955		1.45	9
RESERVOIR ROUTING FOR SUGARHOLLOW LAKE ISTAG ICOMP IECON ITADE		AVG	00.0-	NSTOL	c I
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	657.0	69.	27. 11H.	652. 657.	ELEVL -0.0	CAM DATA CAGO -0.0	STATION OUTING, PLAN 1. RATIO 1	END-OF-PEPIOD HYDROGRAPH OPDINATES	AG.	ċċ	•				. m. ș	17.	25.	34	47.	40.	9.4	96	215.	245	178	124.	126.	119.	116.	A GE		ò		
	651.5 656.5	43.	19. 198.	651. 656.	EXP.	10PEL C	110N OUT	)F-PEP101	0+1TFL9W	••			<b>.</b> .	: :	ะ เพื่อ		25.	33.	, <del>,</del>	5A.	93	96.	206.	258.	194.	130.	126.	120	117.	STORAGE	0	<b>.</b>		
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PEAK OUTFLOW

FND-OF-PERTOD HYDROGRAPH ORDINATES STATION DUTING. PLAN 1. RATIO 2

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OUTE OF		•	6	•	<u>.</u> :	-	_:	ċ	۶.	æ	22.	<b>4</b> 1.	, v.	63.	46	*	84.	101.	118.	221.	1590.	1163.	715.	460.	232.	171.	130.	127	124	122.	STOBAGE			•	; <b>.</b> -		.:	ċ	3.	•	12.	18.	, y	. I.	• ÷		, so	. 711	15.7	201	147	175.
	<	• •	•		<u>:</u>	_:		~:	۵,	7.	20.	39.	53.	63.	69	74.	83,	•66	116.	194.	1486.	1231.	736.	* 66	23A.	177.	134.	127.		122.			•				_:	~	3.	5.	11.	1 <b>A</b> .	24.	÷,	<b>.</b>	•	, e	110		197	, o H C	75.
	c	•	<b>.</b>	•	:	-	-:	۶.	2.	•	18.	37.	54.	62.	58.	73.	B).	٠,٢٥	115.	175.	1342.	1343.	754.	536.	245.	182.	137.	127.	\$	122.		•	•		-		-:	۶.	۶.	'n.	11.	17.	23.	<b>.</b>	ţ;	•	75.	107.	1 4 5	193.	161	176.
	•	•	•	ė	ċ	<b>:</b>	<b>.</b> :	 	ζ.	÷	17.	35.	ŗ	.24	y.	73.	.08	۰,	113.	151.	1163.	1379.	701.	540	251.	. H# .	C 4	129.		122.		Ċ	0		· <u>-</u>		-:	ζ.	2.	;	10.	17.	23.		Ç.		72.	103		197	. 46	177
	ć	•	•	•	£ .	<u>:</u>	-:	۶.	ۀ.	ŗ	16.	33.	***	;	٠,٢٠	77.	78.	۲۴.		130.	943.	1455.	**	546	257.	7.	144.		9	123.		ċ	•	c	<u>:</u>	-	-	· .	٠,	;	٠,	<u>.</u>	22.0	<b>:</b> ;	•		?		1 3 7		100	178.

. 159.	•	141	135	130.	125.							_	_	-			651.3				_	_	_		•		-	_		_						
16.9	150.	141	135,	130.	125.			650.3	650.3	650.3	650.3	650.4	4.059	650.4	450.5	650.A	651.2	651.6	652.0	655.3	652.7	653.0	654.1	655.7	657.6	659.5	661.0	0.099	659.7	659.1	658.6	658.2	657.9	657.6	657.4	
161	151	142.	136.	131.	126.	121.		650.3	650.3	650.3	650.3	4.059	650.4	4.059	650.5	650.8	651.2	651.6	651.9	652.1	455.6	653.0	654.0	655.6	4.159	659,3	1.199	660.1	459.7	659.2	658.6	658.2	657.9	457.7	657.4	457.1
163	152.	143.	137.	131.	126.	121.		650.3	650.3	650.3	650.3	4.054	4.054	4.054	450.5	650.7	651.1	651.5	6-159	652.3	652.6	4.554	653.9	4.55.4	657.2	659.1	1.159	460.2	4.65	2.654	458.1	658.3	457.9	457.7	4.159	6.27.2
164.	153	144	137	132.	127.	122.	w	w	•	•	•	w	w	Ð	•	æ	1,159	•	¥	•	v	ų.		·	æ	v	w.	•	æ	•	w	•	•	4.	•	•
166.	154.	144.	138.	132.	127.	122.	STAGE	650.3	650,3	650.3	650.3	659.4	650.4	4.059	650.5	650.7	651.1	651.5	651.8	652.2	652.5	6.559	653.6	655.1	655.8	658.7	661.0	660.4	659.8	650.3	654,4	658.3	658.0	457.7	657.5	657.2
167.	155.	145.	3.34	133.	128.	123.		650.1	650.3	£ 059	650.3	4.059	650.4	4.054	450.4	9.054	651.0	4.159	651.B	656.2	655.5	852.B	653.5	6.454	456.6	658.5	640.9	650.5	4.55A	3.000	658.9	658.4	654.A	457.4	657.5	657.2
168.	156.	146.	139.	133.	128.	123.		650.3	650.3	650.3	650.3	4.059	4.064	4.054	650.5	4.059	651.0	4.1.4	651.A	452.1	652.5	652.8	653.4	654.7	4.954	55H.4	460.6	650.6	6.646	629.5	658.9	454.4	659.1	657.8	457.5	657.3
169	157.	147	139.	134.	129.	124.		650.3	650.3	650.3	450.3	650.3	450.4	450.4	450.5	450.4	450.9	651.3	451.7	652.1	452.4	4.7.7	F.F34	454.4	454.2	454.2	4.094	464.7	459.9	453.5	450.0	659.5	458.1	A57.A	657.5	657.3
170.	158.	1 & B.	140.	1.30.	129.	124.		650.3	650.3	650.3	654.3	650.3	4.059	450.4	4.054	451.6	6-059	651.3	651.7	652.0	4.254	652.7	653.2	654.4	655.1	654.0	660.1	6.049	6.059	654.5	0°659	658.5	654.1	657.8	657.5	657.3

1667. AT TIME 16.42 HOURS PEAK OUTFLOW IS

TOTAL VOLUME 55962. 1585. 179 121.62 385. 475.	
72-MUH- 194. 6. 4.79 121.62 3A5.	
24-HOUR 194. 6. 4.79 121.62 385. 475.	
6-HOUR 18. 3.45 97.81 330.	
PEAK 1667.	
CFS CNS TNCHES AM AC-FT THOUS CU M	

213. MAXIMUM STORAGE = STATION OUTING. PLAN 1. RATIO 3

			•	7:	<b>:</b> :
		•		-	:
OPDINATES		•	•	-:	<b>:</b>
TOROGRAPH		•			
END-OF-PERIOD HYDROGRAPH ORDINATES	OUTFLOW	•	ċ	<b>:</b>	<u>:</u>
END-0		•	•	-:	<b>:</b>
		•	•	•	:
		•	•	•	-
					•

e e e -

**...**.

:-		3,	æ	24.		76.	82.	.68	96	114.	216.	945	1472	2327	1361	932	•11•		•			• , , ,		•	• •	<b>.</b>	: -	~ ~			ur.	13.	25.	32.	· ·	20.	73.	9	152.	180.	197.	225.			5	145.	139.	۰	2	_	٠,	: -	4.000		6.65	•
:_		3.	۲.	25.	•	, F	89.1	AB.	95	112.	168.	126	1298.	2433.	_	400		. 102	• • • • • • • • • • • • • • • • • • • •	196.	127	121		<	;	<b>.</b>	: -	. ~		'n	` <b>v</b>	12.	21.	31.	• •	. 19	71.	102.	147.	179.	107		193	165	154.	145.	140.	136.	136.	Š		2 6	650.4	50.		•
:-		3.	•			72.	80.	<b>88</b> .	3	2	159.	5	11	2517.	200	2		- 6	Ų L	190	127	125.		•	•	; -				m	\$	11.	29.		•	90.9	70.	96	Š	177.	187.	100	182	167	55	146.	4	9	133.				4.064	:		
		3.	ທ໌	1.	6.5	7	80.	. 18	• • •	108.	130.	25	707	.1057	ב ה			187.			127	125.		ě	•	-	: :			m m	÷	<u>.</u>	.61		• • • • • • • • • • • • • • • • • • •	. 56	•69	94.	138.	175.	185.	200.	183.	169.	156.	147.		137.	129.	50		2 2	4.20.4	9	650.	
	~	ë,	'n	•	-	7	79.	35.	93.		127.	0,0	1076	.5.67	600	• • • • • • • • • • • • • • • • • • • •	240	192	16.2	124.	127.	125.	96		•			-	67	3.	÷	•	• •		• T	58.	5B.	91.	2	9	4 1	20.3	184.	=	2	14H.			139.	654.	50.	. 5	4.059	50.	59.4	ſ
1-	2.	3.	ທໍ່	• 6 6		70.	78.	86.	6	2 6	471		* *	C 4		- 4	) u	6	ď	5	128.	9	840013	<u>۔</u>		-	: -	-	~	æ,	÷	ė į			47.	57.	47.	. 18	129.	170.	E 6	206.	3	172.	S.	9	100	: :	130.	5	20	50.	650.4	50.	59.	
: -	2	<b>.</b>	• ;	35.	58°	69.	77.	85.		193	166.		1001	125	, ,	***	277.	202		3.30	128.	126.		9	•	: :	: <b>-</b>	-	ď	3.	•	œ į	17.		• •	56.	66.	3	123.	167.	225	210.	185.	174.	154.	140			131.	50.	59.	50.	4.059	50.	50.	
	۶.	۶.	• ;	33.	56.	6 H.	۲.	* 30 3	•		16.5		210	147)		0 4 2	306.	207	162.	132	178.	126.		ċ	•	: -:	-	-	۶.	3.	•	• ;	<u>.</u>	35.		55,	65.	81.		194.		213.	188.	176.	160.	150.		1 20	131.	_		_	4.059		4.054	
	~	٠.	• •	9.0	54.	67.	76.	a c	. 00			000	1000	2089.	1243	40.	334	213.	146.	. 34.	124.	124.		0		•	-	-:	٠,	3.	<b>4</b> (	- 4	· · ·	<b>,</b>	•	54.	, <del>, ,</del>	4.	<u> </u>		- L - C - C - C - C - C - C - C - C - C	217.	190.	7	<u>.</u>	151.			131.	450.1	450.3	450.3	450.4	450.4	4.054	
<b>:</b>	ς.	ů.	• 0	٠٢2	٠ د د	,44	٦٥.	e d	4	118.	243.	970	1641	2209	1300	-	373.	217.	176.	137.	124.	126.		•	ċ	•	<u>:</u>	:	ζ.	<b>.</b>	. م	;		, E	<b>4</b> 3.	5.4	• •	5.	÷ 4		101	221.		17H.	162.	, , , , , , , , , , , , , , , , , , ,	90	3.5	132.		-	650.3	650.3	650.4	650.4	

· C	150.5	650.5	650.5	650.5	650.6	650.6	650.6	650.6	650.6	650.6
•					6 6 6	0 427	0 437			461
ď	550.7	- One	0000	2000	0000	. 0.0		24160	1 • 1 6 6	1.100
•	151.2	451.2	651.3	651,3	651.4	651.5	651.5	651.6	551.6	651.7
•	151.7	451.4	6.169	6.159	652.0	652.0	652.1	652.2	652.2	652,3
•	152.3	452.4	4.259	652.5	652.6	652.6	452.7	652.7	652.8	652.9
•	152.9	653.0	653.0	653.1	653,1	653.2	653.3	653,3	653.4	653.4
•	153.5	453.5	453.5	653.7	653,7	653.A	653.B	653.9	653.9	654.0
•	154.0	1.454	654.2	654.2	654.3	654.3	4.459	654.5	654.5	654.6
•	8.45	454.9	655.0	455.2	4,559	655.6	655.8	656.0	656.2	656.4
•	9445	454.9	657.1	657.3	657.5	657.7	658.0	658.2	658.5	658.7
•	4. Kil.	450,1	6.44.9	4.659	659.6	6.69.7	6.59.8	6.659	650.0	660.0
•	140.1	460.1	650.1	660.1	5,099	660.2	660.3	4.094	9.099	660.B
•	1919	461.5	A61.8	662.1	662,3	4.299	652.4	462.4	662.3	662.1
•	61.9	461.7	661.6	661.4	661.2	661.1	661.0	6.04	660.8	1.099
•	9.095	460.5	4.094	6.064	660.3	660.2	5.099	660.1	660.1	660.0
•	150.0	459.9	654.A	659.R	659.7	659.6	6.69	659.4	659.3	654.3
£	5.455	459.1	659.1	659.0	659.0	654.9	6.88.9	658.8	658.8	658.7
•	558.7	45A.7	65A.6	65H.6	658.5	658.5	658.5	4.859	658.4	658.3
•	554.3	454.3	654.1	65H.2	659.2	658.2	658.1	658.1	658.1	658.1
•	558.1	454.0	658.0	654.0	658,0	659.0	6.754	657.9	657.9	657.9
•	557.9	457.9	A57.8	657.A	657.8	657.8	657.8	657.7	657.7	657.7
•	557.7	657.7	657.7	657.6	657.6	657.6	657.6	657.6		
•••	55 x . 1 55 7 . 9 55 7 . 7	454.0 457.9 657.7	658.0 657.8 657.7	654.0 657.8 657.6	658.0 657.8 657.6	659.0 657.9 657.6	657.9 657.8 657.6	657.9 657.1 657.6	Ø &	557.9

TOTAL VOLUME	91469.	2590.	7.93	198.79	630.	111.
72-HOUR	318.	•	7.83	19A.79	630.	.111.
24-HOUR	318.	•	7.83	198.79	ń30.	177.
6-HOUR	1082.	31.	99.9	169.24	536.	•299
PEAK	2561.	73.				
	CFS	570	INCHES	¥	AC-FT	THOUS CU M

MAXIMUM STORAGE = 232.

STATION OUTING. PLAN 1. RATIO 4

END-OF-PERIOD HYDROGRAPH ORDINATES

	•	1.	-	-:	4	e e	•	11.	34.	62.	75.	9¢.	95.	163.	112.	. R3.	984.	1303.	1968.	
	•	•	-	٦.	۶.	m m	s,	10.	33.	61.	74.	85.	94.	103.	111.	151	947.	1275.	1736.	į
	•	•	-:	-	۲,	e,	เก	•	30.	50.	73.	94.	93.	102.	110.	129.	808.	1244.	1577.	;
	•	•	-:	-	۶.	ë.	2.	<b>.</b>	26.	57.	71.	83.	95•	101	109.	126.	742.	1213.	1479.	i
	•	•	-	<b>:</b>	۶.	e e	;	•	23.	54.	70.	A2.	91.	100.	104.	123.	645.	1180.	1428.	
OUTFLO	•	•	-	-	۶.	۲.	;	,	20.	51.	.69	. 18	91.	99.	107.	121.	575.	1144.	1402.	
	•	•	<b>:</b>	-:	۶.	۶.	;	۲.	18.	<b>*</b> 6 <b>*</b>	6.8°	79.	<b>.</b> 06	<b>.</b>	107.	- 10	472.	1115.	1385,	
	•	•	<b>:</b>	.:	-:	۶.	<b>;</b>	•	16.	<b>4</b> 6.	<b>.</b> 49	78.	89.	98.	106.	117.	352.	1044.	1369.	
	ċ	•	-	<b>.</b>	-1	۶.	3,	ý	÷.	43.	.55	77.	A.	97.	105.	115.	24H.	1053.	1350	
	•	ė	-:	-	-	<b>ئ</b>	3.	÷	12.	•	••	74.	¥7.	ç,	104.	<u>:</u>	216.	1029.	1324.	
																				i

i																																																										
1964.	ë.	=	543	520	245	•	162	•	139			٠.	-	•	-		-	;	7.	17.	20.	<b>6.3</b>	57.	71.	Š	162.	9	181.	5	213.	6	5 6		156.	148.	143.	139.	137.			650.3	6.50.3	650.4	*****	4 6 6 6	6.00	650.B	651.4	652.1	652.9	653.7	654.3 C. 403	6.56.2	4	660.1	660.6	661.6	663.3
736	245	1902.	283	280	24B.	198	165.	142.	1 30.			•	-	-	-			;	7.	16.	28.	42.	56.	.0.	÷	3	:	180.	191.	200.	255.		141	157	149.	143.	140.	137.			650.3	650.3	650.4	1000	4	650.6	650.7	651.3	652.0	652°B	653.6	404.4	656.0	658.2	660.0	660.5	661.2	563.5
577	3356.	997	330	35	3	2	9	:	130	,		•		: -	: -:			;	ċ	15.	27.	<b>4</b> 0.	24.	69.	A3.	97.	136.	178.	100	200°	254.			15.6	140	144.	140.	138.	136.		50.	20.	9			20.	50.	51,	52.	25.	23	. u	200	57.	629.9	60.	3	663.6
1479.	3416.	2101.	1372.	464	767.	207	170	•	900			•	•		-			;	•	.*.	24.	39.	53.	67.	81.	95.	131.	176.		197.	260.			150.	150.	144	.04	136.	136.		650.3	650.3	9.000	4.000	450.5	650.6	K50.7	651.2	6.159	652.7	653.5	2.406	A 45. R	657.6	6.59.8	4.049	4.057	663.7
1428.	3402.	2216.	1418.	157.	295.	212	173.	148.	136.	•	'n.			-	:	,			ŗ	12.	24.	38.	51.	.99	80.	• • •	126.	173.	187.	ç	760	7	145	150.	. 151	145.	141.	136.	136.		•	650.3	650.4	4.000	2.059	650.5	650.6	651.1	651.9	652.6	653.4	654.6	455.7	657.4	659.7	640.4	6.059	643.7
1402	3345.	2342.	1468.	619.	326.	216.	176.	150	133	153	STORAG			: -:	: -				5.	-	73.	36.	20.	•	78.	60	121.	170.	186.	195	. 25.		751		152.	145	141.	134.	136.	STAGE	~	650.3		4.000											689		660.7	663.6
1385	3127.	2480.	1525.	<b>626</b>	360.	221.	. 89.	.25	134	• • • • • • • • • • • • • • • • • • • •		ė	<i>-</i>		: _			;		19.	22.	35.	<b>*</b> 8	63.	.77	91.	116.	166.	185.	36.0	.152		· ·	162	.52	146.	141.	134.	136.		650.3	650.3	550.3	*****		650.5	650.6	651.0	451.7	455.4	653.7	6.414	455	6.96.9	659.4	640.3	660.7	663.3
1369.	2876.	.6292	1544.	1957	397.	224.	. B 3.	155.	136.	•		•							\$	•	21.	33,	.1.	61.	75.	.06	112.	162.	4 X Y	4 C	£43.	201		153.	153.	146.	142.	139.	137.		650.3	650.3	659.3	4.004	4	650.5	650.6	650.9	451.6	652.4	653.2	634.0	45.4	656.7	659.7	660.2	640.7	662.9
1350	2575.	2786.	1658.	1124.	417.	271.	197.	157.	137.	•		c	· c	ئے '	: _:	: .		' م		•	.61	32.	*4	٠,	74.	a a	104.	157.		143	233			44		147.	142.	173.	137.		650.3	450.3	450.3	970.4	4.054	650.5	650.6	650.A	651.5	652.3	653.1	65.4	4.55	656.5	458.9	469.2	4.054	A62.5
1328.	2259.	5946-	1737.	1100.		237.	140		139	• 6 9 1		ċ	ی	-	-			,.	\$	æ	· ·	31.	**	SB.	73.	87.	105.	152.	. A.Z.		243			166.	1 4 4 1	147.	147.	134.	137.		650.3	650.3	650.3	4 0 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4.054	650.5	650.6	650.8	651.4	652.2	653.0	456	4.00	656.3	654.7	660.1	4.044	662.0

	463.4	4.5.4.4			. 644	0 177	44114	7 177		
	700	0.000		0.360	1000	100	100	000	6 1 40	
	651.2	451.1	991.0	640.0	9.099	2.699	660.	9.059	660.5	660.5
	4.059	660.3	669.2	660.1	660.0	629.9	459.8	659.7	9.659	459.5
	4.459	459.1	659.2	659.2	659.1	659.1	659.0	659.0	658.9	658.9
	6.459	454.8	458.8	454.7	658.7	649.6	658.6	658.6	45A.5	A5A.5
	654.5	45A.4	65H.4	65H.4	454.4	654.3	658.3	654.3	4511.3	65A.3
	654.2	45A.2	658.2	458.2	658.2	654.1	658.1	.658.1	658.1	65A.1
	654.1	454.1	658.0	658.0	458.0	659.0	658.0	658.0	658.0	658.0
	654.0	454.0	657.9	6.754	6.1.9	6-159	6.759	6.129		
AK OUTFLOW	18	3416. AT TIME	16.42	5dH04						

MAXIMUM STORAGE # 26

1538. 1538. 44. 9.47 240.66 753.

CFS CHS CHS INCHES MA AC-FI THOUS CU H

PEAK 3416. 97. STATION OUTING. PLAN 1, RATIO 5

END-OF-PERIOD HYDROGRAPH ORDINATES

	•	<b>:</b>	:	٠.	ζ.	5.	ě	:	47.	70.	ž.	94.	107.	116.	126.	736.	1317.	1638.	2461.	3879.	2268.	1554.	644.	255	212.	187.	161.	150.	
	•	<b>-</b> :	٦.	۶.	۶.	;	7.	13.	;	68.	H3.	45.	106.	115.	124.	647.	1283.	1605.	2172.	4056.	2378.	1611.	704.	272.	216.	185.	164.	151.	
	•	-	-:	۶.	2.	;	7.	12.	<b>*</b> 0	<b>9</b> 9	<b>8</b> ].	94.	105.	114.	123.	546.	1251.	1570.	1973.	4196.	2497.	1663.	769.	29A.	220.	187.	166.	152.	143.
	•	-:	:	-:	2.	÷	۲.	11.	36.	65.	80.	93.	104.	113.	122.	431.	1214.	1534.	1951.	4270.	2627.	1715.	A37.	329.	224.	190.	168.	153.	144.
																												154.	
OUTFLO	•	ċ	<u>.</u>	-	۶.	ë.	÷	10.	28.	62.	77.	90.	101.	112.	120.	234.	1129.	1462.	1756.	4132.	2927.	1835.	1120.	401.	232.	195.	171.	154.	145.
	ċ	•	:	-	۶.	'n.	<b>.</b>	ċ	24.	.09	76.	.68	100.	111.	120.	201.	1081.	1429.	1735.	3909.	3099.	1904.	1223.	442.	236.	100.	173.	157.	144.
	•6	•	:	نہ	۶.	ë.	٠,	•	21.	56.	<u>.</u>	98.	•66	110.	119.	170.	1028.	1397.	1716.	3595.	3246.	1985.	1321.	487.	241.	202.	175.	158.	147.
	•	•	-:	<b>:</b>	۶.	٦.	'n.	€		53.	73.	<b>.</b>	80	109.	118.	141.	972.	1364.	1694.	3220.	3443,	2472.	1410.	515.	246.	205.	174.	140.	144.
	•0	•	-	<b>:</b>	٠,	÷	ۍ.	į	16.	50.	<u>:</u>	<b>6</b> 5.	97.	104.	117.	128.	A16.	1341.	1664.	2424.	3443.	2164.	34 F 3 .	547.	.055	20B.	-111	141.	149.

	ċ	-	-			•	• 4	rc		- 2	4		· ~		•	- 7 -	• • • •		20%	229.	273.	223.	20u•	172.	15.A.	151.	144.	143.	141.			650.3		5 C C C C C C C C C C C C C C C C C C C	4 6 6 7	1 of 10 of 1	0.00	0.00	0.000	45.15	652.6	653.6	654.6	655.6	656,6	657.7	659.A	640.6	661.1	5.740	669	6.049	659.7	659.0	658.6	458.4	658,3	658.2	
	•	٠,	1.		,,,	; 4	• 4	n e		, c			3			140	• 77.1	191	201	550	281.	226.	.201.	174.	159.	152,	147.	143.	141.			450.3	6.000	4.000	4.000	4 6 6 6	650.5	9.00	4	4.5	652.5	653.5	654.5	655,5	656.5	657.5	659.7	660.5	0.199	6-100	662.2	661.0	659.8	659.0	454.7	65H.4	658.3	658.2	
	•	-	-			•	• 4		• •					306	•	627	* of o		002	213	245.	230.	203.	177.	160.	.55	147.	144.	141.	140.		6603		4.000	4 6 6 4	4.04	4	4.000	9 0 0 9 4	451.4	452.	653.4	654.4	4.829	4.954	4.759	659.5	660.5	661.0		662.4	661.1	6.959	659.1	658.7	658.5	65A.3	658.2	
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36	•		_			•	• •		- u			. 54			•	•	•	181	96	207	281.	239.	50 Y •	182.	162.	153.	148.	144.	142.	140.	L			4.059	4 054	4.029	40.00	6.034	650	651.3	6.55.0	653.2	654.2	655.2	656.2	657.2	650.1	660.4	640.4	6.100	6.000 8.000	66199	560.1	659.2	65A.B	654.5	658.3	658.2	
STORAG		ċ		: -:		٠,	* .	'n	• • •	. 0	• · ·					•	•		147	. 902	283.	244.	<b>508</b>	186.	163.	154.	.48.	144.	142.	140.	70470			\$ 45 Y	4 6 6 6	650	4	4	6.66	, LT.	65.2	653.1	654.1	655,1	656.1	657.1	6.859	669.3	660.8	2.100	664.0	4.(99	660.3	659.2	658.A	65H.5	6.58.3	658.2	
	ć	6	-	-	• •	: ,	• •	•	• •		• •	ç			:	• • • • • • • • • • • • • • • • • • • •	•	104	196	206.	276.	250.	211.	169.	165,	155,	140	165,	142	140.		450.3		456	4.5.0	4.054	4.00	0.054	650	1.154	6.52	653.0	654.0	655.0	656.0	657.0	658.6	640.2	8.0.3	2.146	664.3	661.5	4.044	659.3	458.A	458.5	458,3	658.7	• •
	ć		: -	-	• ,	ζ,	<b>,</b>	* •		34.6							• • • • • • • • • • • • • • • • • • • •	5 K 7	195	205	244.	256.	214.	142.	166.	156.	144.	145.	142.	140.		450.3	6.00	4.054	4504	4.054	, n		450.7	651.0	9,159	6.559	623.9	6.459	6.554	6.959	654.3	650.2	660.7	2.1.0		661.6	669.6	659.4	659.0	63A.A	45H.4	658.2	•
			•		• •	••		•	•	• 1.6	•	a U						141	104	502	524	267.	216.	194.	149.	154.	154.	145.	143,	141.		650.3	450.2	, C.S.	4 0 11	4.054		4.054			651.8	452.A	653.8	654.8	654.4	654.A	45P.1	1.099	650.7		6.69.	461.7	460.7	A50.5	A5A.4	454.6	45H.4	458.2	:
	•	ć	`-	•	• .	• 1	•		•			4	. *	. 5						2.3	24.	569	2	197.	174.	1,7	156.	146.	143.	101.		450 3		6.00	4 054	4.054	6.000	4.0.4	650.7	5 659	651.7	652.7	653.7	654.7	654.7	454.7	6.259	660.0	0.076	1.100	6.444	6.199	660.8	659.6	658.9	65H . 6	654.4	654.2	

TOTAL VOLUME	163388.	4627.	13.94	355.09	1125.	1388.
72-H0U4	567.	16.	13.98	355.09	1125.	1348.
24-HOUR	567.	16.	13.98	355.09	1125.	1388.
6-HOUR	1978.	56.	12.19	309,55	441°	1210.
PEAK	4270.	121.				
	CFS	CMS	SHOWE	3	AC-FT	THOUS CU M

288. MAXIMUM STORAGE =

STATION OUTING. PLAN 1. RATIO 6

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	9.059		9.059	-	9.059	450.6	650.6	650.6
	450.7		650.7	-	4.059	450.7	650.A	550.B
	650.8		6.059	_	650.4	4.054	620.9	651.0
	651.0		651,1	651.1	651.1	651.2	651.3	451.4
	651.7		655.0	_	655.3	652.5	652.6	652.A
	453.4		653,8	-	654.2	454.4	654.6	554 . A
	454.4		655.8	-	6.56.2	656.4	656.6	616 816
	4.759		657.A	_	658.2	654.4	658.5	658.7
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	6.659		629.9	_	459.9	6.659	90099	660.1
	650.5		650.A	_	661.1	661.3	661.4	651.5
	6.179		662,1	_	662.3	462.4	667.5	902.0
	46%.8		663.0	_	663.2	643.3	663.4	663.5
	463.8		6.1.9	_	464.2	464.5	665.1	666.0
	46.19		671.0	_	4.1.4	671.2	670.B	670.2
	66.8.5		667.4	_	6.96.5	466.1	665.7	565.4
	464.6		664.1	_	663.7	663.6	663.4	663.3
	662.6		662.0	-	461.4	651.1	460.A	650.6
	460.1		659.8	_	4.654	659.5	659.4	459.4
	459.2		659.2	-	659.1	1.659	659.1	654.1
	459.0		659.0	-	659.0	459.0	659.0	654.0
	A59.0		659.0	_	6.654	6.59.0	659.0	6.659
	4.89.0		659.0	-	0.659	0.659	659.0	650.0
	655.0		659.0	_	659.0	659.0		

PEAK GUTFLOW IS 9540, AT TIME 16.42 HOURS

CAS	8540. 242.	4005. 113.	24-HOUR 1196. 34.	1196.	707AL VOLUME 344476. 9754.
INCHES CM AC-FT THOUS CU M		24.67 626.65 1986. 2449.	74.47 744.64 2372. 2926.	2372° 2372° 2926°	74.47 748.64 79.72 .9926.

SUB-AREA RUNDEF COMPUTATION

									COMP 0	379.	<b>*</b> 04	526.	618.	607.	RB7.	952.	1035.	1063.	1112.	1140.	1174.	1248.	1292.	1311.	1335	1366.	1377.	1389.
1±UT0 -0			110 10				VOL= 1.00 460. 28. 21.		5507					100		ē.		٠ <u>٠</u>										
	LOCAL		RT1MP . 10				VOL #	-:	EXCS	.20	2.0	202	.20	7 7	.2	2.2		2.5	25.	.25	52.	2.5	.25	25.		S.	. 25	٠ <u>.</u>
E ISTAGE	ISAME L	R96 -0.00	ALSMX -0.00				577. 577. 36.	۲,	RAIN	.22	22.	22.	-22	2 2	2	25.	.25	25.	, ç	56	92°	, s	\$	۶,۶	÷ ×	. &	.26	35
INAME		٩	CNSTL -82.00			00.	. LAG=		PERIOD	145	9 7	148	149	151	152	153	155	156	158	159	99.	162	163	164	165	167	168	169
JPRT 3	I Sr	8 R72	STRTL -1.00	82.00		RIIOR# 3.00	-0.00 HOURS, LAGE 664. 5.	e e	HR. HN P	12.05	12.10	12.20	12.25	12.35	12.40	12.45	12,55	13.00	13,10	13.15	13,20	13,30	13.35	13.40	13.45	13,55	14.00	14.05
JPLT	RATTO -0.000	948 00.00	RTIOK 1.00	N S	ATA S	9	~ .	4	٧	1.01	٥٠. د د	1.01	1.01	10.1	1.01	1.01	1.0.	 	1.01	1.01		1.01	1.01	10.1			 	
BINHOOD ON 11APE -0 -0	HYDROGRAPH DATA TRSDA TRSPC *72 1.00	PRECIP DATA R12 R24 120.00 130.00	LOSS DATA STRKS -0.00	-1.00 EFFECT CN	UNIT HYDROGRAPH DATA 0.00 LAG≈ .45	RECESSION DATA DACEN	ES+ TC	ė į	END-OF-PERIOD FLOM COMP G MO.	1,	,	, m	ຕ້	ř vň	· \$	* -	7.	œ° œ	. 60		<b>.</b>	• ec	. 60	æ í	œ° œ	• • •	· ec	
SUBAREA RUNDFF FOR LAKE ROBINHOOD ISTAO ICOMP 17.	SNAP HY	R\$ 100.00 12	L ERAIN 0 -0.00	и	UNIT	1.44 A	PERIOD 556. 110.		LOSS CO	.01			.01		10.	5	. ē.	5.5		10.			.01	10.	10.0	: <del>-</del> =	.01	.01
A RUNDFF FO ISTAD IC Inflow	TAREA . 72	PMS 26.00 1	KH RTIOL 00 1.00	.00 WETNESS		STRTO=	29 END OF 344. 146.	<b>.</b>	EXCS	00.	000	00.	60.		00.	000	00.	2.5	9 0	00.	9	9 9	00.	00.	0 0	. 00	00.	00.
BAREA I	IUHG 2	SPFE-0.00	DL TKH -0.00	≥ -82.00					RAIN	.01	ē.		10.		.01	10.	~ ·	5	-	.01	.0.		ī .	.01	6.0		.01	6°
Sul	IHYNG 1	* 7	STPK9	CURVE NO 3			UNIT HYDROGHAPH 168. 189.	12.	PER10D	-	۸ ۴	? ∢	<b>د</b> د	۰ م	Œ	٥ ۾	=	2.5	: ≾	۲.	<u> </u>	<u>.</u> .	2	۶,	2 2	38	*	22
			LR0P1 -0	U			55.	.95	AN. M.	50.		2.	52.	3.0	04.	4 n	\$5.	00.1	1.10	1.15	1.70	98.	1.35	64.	V	1.55	5.00	2.05
								•	40.04	1.01	16.1		.00		1.01	6.6	10.	3.5		10.1			10.1	1.01		: E	1.01	1.01

2.05 1.01

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• 02	.02	~ O.	20.	20.		.02	.02	20.	20.	٥٥	<u>د</u> د	٠٠.		C .	\ c \ c	\ c •	200	20.	20.	0.0				60	20.	÷0.	- 02	.02	. 0 <b>.</b>	20.	20.	20.0		-0.	- 05	20.		2 6		- 02	-05	-05	- 05	20.		•			-02	33.80 31.55 (859.)(801.)
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19,30	19,35	19.40	19,45	14.50		20.05	20.10	20.15	20.20	20.25	20.30	20,35	20.40	20.45	05.0%	56.02	٠.	51.15	:.	21.15	21.00	62.12	21.15	21.40	21.45	21.50	21,55	22.00	55.05	22.10	22,15	22.20	22.30	22,35	22.40	22.45	22.50	66.55	23.05	23,10	23,15	23.20	23,75	23.30	63.50	D	23.43	23.50	00.0	
1.01	1.01	1.01	.00				1.01	.03	1.01	 	1.01	1.01	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1				10.1	16.1	1.01	1.01	1.01	1.01	10.1	ē.	10.		.0.	1.01	1.01	1.01			1.0	1.01	1.01	1.01	: ·	7		10.		1.02	
261.	267.	273.	27A.	283.	250	294.	300.	303.	307.	319.	313.	316.	319.	321.	324.	326.	324.	111.		333	936	37.0	0.00	3, 10	345.	346.	348.	34.3.	351.	352.	353.	404°	356.	35A.	354.	360.	361.	361.	364.	364.	365.	366.	366.	367.	366.	. 60.6	.00		371.	
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. 07	10.	.07	6	.00			.07	-03	.0.	-01	. 07	.07	.0.	- 0.7	, ii ,		20.	/0.		10.					. 0	.07	.07	.07	٠٠٧	.07	-0.			.0	.07	· 0.7	20.	- 0 -		. 0.	.07	.07	.07	-0.			5 6		.07	
96	6	92	e 6	9. Q	, 6	9.	æ	66	100	101	102	103	104	20.	105	101	* 6	0 0		- :			• 4		117	118	119	120	121	122	123	4 0		127	124	150	0 F F		<u>}</u> :	1 14	135	136	137	134	9 F T		141	142	14.	
7.30	7.35	7.40	7.45	7.50	3	8.05	8.10	8.15	9.20	8.75 5.5	9.30	9.35	0	6.45	α: α:	τ. υ.	00.6	n .	01.	r :		0.00	9	24.0	6,45	٠,	9.45	10.00	10.45	10.10	10.15	01.01	10.30	10.35	10.40	10.45	10.50	10.01 0.00		11.10	11.15	11.20	11.25	11.30	11.35	11.0		7.50	12.00	
1.01	1.01	1.01	1.01		-		1.01	10.1	1.01	1.01		1.01		-	19.1	1,	10.1			 					10.1	1.01	1.01	1.01	1.01	1.01		10.1		10.1	10.1	10.1	1001		-		1.01	10.1	10.1	 	10.1	10.1	0.0		1.01	

CFS 5563. 1941. 610. 610. 175780. CFS 158. 55. 17. 4978.

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31.54 Ini.16 1211. 1493.	17578. 17578. 3.18. 30.12. 121.	996. 996. 6.31 160.24 242. 299.	VOLUME 52734. 1493. 9.46 240.35 363. 448.	VOLUM 70312 1991 12.6 320.4 484
	1 FOTAL	0 2 TOTAL	R710 3	RTIO 4 IR TOTAL 25 27 27
31.54 801.18 1211. 1493.	PLAN 1, RTIO T2-HOUR 61. 2. 3.15 89.12 149.	PLAN 1. RTIO 72-HOUR T 122. 3. 6.31 160.24 242. 799.	72-HOUR 183. 183. 9.46 240.35 363.	PLAN 1. RTIO 72-HOUR 244. 12.62 320.47 597.
31.54 801.18 1211. 1493.	STAINFLOW FOR PL OUR 24-HOUR 94. 61. 5. 51 3.15 .51 80.12 96. 121.	FOR 10UR 3. 3. 3. 3. 242. 242. 299.	STAINFLOW FOR F OUR 24-HOUR 87. 193. 16. 5. 52. 65. 240.35 89. 448.	STAINFLOW FOR 76, 76, 74, 74, 73, 320,47, 73, 320,47, 697,
25.07 636.83 962. 1187.	6-H	6-HOUR 24-15 11.5-01 127-37 166 237.	AT 6-H 5 5 191	6-H 7 7 255
	HYDPOGRAPH PEAK 556. 16.	нүородалрн Р <u>ғак</u> 1113. 32.	нуоробрарн Реак 1669. 47.	HYDROGRAPH PEAK 2225. 63.
INCHES IN AC-FT HOUS CU IN	CFS CAS CAS TACHES AC-FT	CFS CMS INCHES INCHES AN AC-FT	CFS CMS TNCHES FM AC-FT THOUS CU H	CFS CMS INCHES MES

101AL VOLUME B7890. 2489. 105.77 400.59 605.

12-HOUR 305. 9. 15.77 400.59 505.

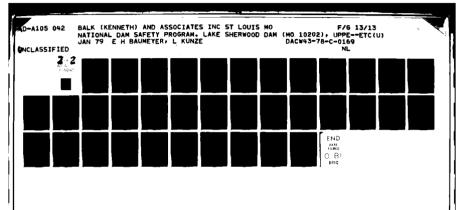
24-HOUR 305. 15.77 400.59 605.

6-HOUR 970. 27. 12.54 318.42 481. 593.

> CFS CMS CMS INCHES AM AC-FT THOUS' CU

PEAK 2782. 79.

HYDPOGRAPH AT STAINFLOW FOR PLAN 1. RTIO S



HYDROGGAPH AT STAINFLOW FOR PLAN 1. RTIO 6

TOTAL VOLUME	175780.	31.54	901.18	1211.	1443.
72-H0UR	610.	31.54	801.18	1211.	1493.
24-HOUR	610.	31.54	801.18	1211.	1493.
6-HOUR	1941.	25.07	436.A3	962	1147.
PEAK	5563,	•			
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ROUTING
HYDROGRAPH

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			656.0	A3.	•	657.						•	•	•	ċ	÷	•	•	:
IAUTO -0			655.0	55.	78.	656.						•	•	•	•	•	•	•	-:
INAME ISTAGE	LSTR -0	STORA 15PRAT-6481		<b>.</b> 8•	.19	655.	ExPL -0.0					• •	•	•	•	•	•	•	•
INAME 1		STORA -648.	454.0	•	56.	654.	CAREA E			ES	·		•	•	-		•		_
JPRT 3	TPHO 1	TSK -0.000	653.0		• • •	653.	COOL C.	DAMVIO -0.	STATION OUTING, PLAN 1. RATIO 1	END-OF-PERIOD HYDROGRAPH ORDINATES	•	: :	•	ċ	•	0	•	ċ	•
JPLT	1097	× 000 • 0-	652.0 662.0	33. 2995.			ELEVL (	DAM DATA 199 EXPD 10 -0.0	PLAN 1	/DR/JGRAP	•		•	•	•	ċ	0	•	-
IOSINHOOD ITAPE	RES ISAME	AMSKK -0.000			36. 154.	652. 662.	EXPW EL	ខ្លុំ	OUTING	ERIOD HY	OUTFLOW	• •		•	ċ	•	•	•	-
IECON	•	LAG -0	651.0 661.0	23.	26.	651. 651.	0.0 -0.0	10PEL 655.2	STATION	END-0F-P		•	•	•	•	•	•	•	
UTING FO ICOMP	AVG -0.00	NSTDL -0	650.0 660.0	11.	17.	650. 650.	SPWID 0.0-				•	<b>,</b>	•	_	•	-	•		_
RESERVOIR ROUTING FOR LAKE ROBINHOOD ISTAO ICOMP IECON ITAPE OUTING 1 -0	CL055	NSTPS 1	<b>649.0</b> 659.0	3.	9. 114.	649.	CREL SP				•	•	•	•	•	ċ	•	ċ	ċ
PESE	0.0- -0.0						<b>.</b> 3				,			ċ	ċ		ċ	•	•
			648.1 058.0	0. 371.	102.	649.						: :	:	•	•	•		•	·
			STAGE	FLOW	CAPACITYS	ELEVATION=													

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PEAK OUTFLOW IS 130. AT TIME 18.17 HOURS

TOTAL VOLUME RB65. 251. 1.59 40.40 61.
72-HOUR 31. 1.59 40.40 61.
24-HOUR 31. 1.59 40.40 61. 75.
6-HOUR 87. 20. 20.49 43.
764K 130.
CFS CAS INCHES NH AC-FT

MAXIMUM STORAGE # 83.

STATION OUTING, PLAN 1, RATIO 2 END-OF-PERIOD HYDROGRAPH OPDINATES

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	•	•	;	•	•	ċ	•	<b>:</b>			•	10.	15.	20.	24.	35.	<b>\$</b>	63.	184.	155.	403.	319.
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													13.									
OUTFLOW	•	ċ	ó	•	•	•	ċ	•	-	2	5.	•	13.	18.	23.	31.	43.	53.	124.	.410	469.	334.
	•	•	•	•	•	•	•	•	-	<b>%</b>	3,	ě	12.	18.	25.	39.	<b>*</b> 5*	52.	11.	771.	*5B.	344.
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PEAK OUTFLOW IS 1444. AT TIME 16.17 HOURS

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FND-OF-PERIOD HYDROGRAPH ORDINATES STATION CUTING. PLAN 1. RATIO 4

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\$\text{STAFE}\$  \text{Affe}\$  \text{Affe}\$	74.	*	.*.	73.	73.	73.	73.	73.		
A4P.1         64B.1         64B.2         64B.2 <th< th=""><th></th><th></th><th></th><th></th><th>STAG</th><th></th><th></th><th></th><th></th><th></th></th<>					STAG					
A48.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2 <th< td=""><td>649.1</td><td>64P.1</td><td>648.1</td><td></td><td>648.1</td><td>_</td><td>648.1</td><td>648.1</td><td>648.1</td><td>448.1</td></th<>	649.1	64P.1	648.1		648.1	_	648.1	648.1	648.1	448.1
648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.1         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.3         648.3 <th< td=""><td>648.1</td><td>A48.1</td><td>648.1</td><td></td><td>648.1</td><td>•</td><td>448.1</td><td>648.1</td><td>648.1</td><td>648.1</td></th<>	648.1	A48.1	648.1		648.1	•	448.1	648.1	648.1	648.1
648.1         648.1         648.1         648.1         648.1         648.1         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         650.4         650.4         648.3         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8 <th< td=""><td>64 A. 1</td><td>54P.1</td><td>644.1</td><td></td><td>648.1</td><td>•</td><td>648.1</td><td>648.1</td><td>648.1</td><td>648.1</td></th<>	64 A. 1	54P.1	644.1		648.1	•	648.1	648.1	648.1	648.1
648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.2         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3 <th< td=""><td>644.1</td><td>648.3</td><td>644.1</td><td></td><td>649.1</td><td>_</td><td>648.1</td><td>648.1</td><td>648.1</td><td>64B.2</td></th<>	644.1	648.3	644.1		649.1	_	648.1	648.1	648.1	64B.2
KAN,2         KAN,2         KAN,2         KAN,2         KAN,2         KAN,2         KAN,2         KAN,3         KAN,3 <th< td=""><td>649.2</td><td>44B.2</td><td>648°2</td><td></td><td>648.2</td><td>_</td><td>648.2</td><td>648.2</td><td>648.2</td><td>648.2</td></th<>	649.2	44B.2	648°2		648.2	_	648.2	648.2	648.2	648.2
648.1         648.3         648.3         648.3         648.3         648.4         648.4         648.4         648.4         648.4         648.4         648.5         648.5         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         648.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3         658.3 <td< td=""><td>544.2</td><td>648,2</td><td>643.2</td><td></td><td>648.2</td><td>_</td><td>648.2</td><td>648.2</td><td>648.3</td><td>648.3</td></td<>	544.2	648,2	643.2		648.2	_	648.2	648.2	648.3	648.3
648.4         648.4         648.4         648.4         648.5         648.5         648.5         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         648.6         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3 <th< td=""><td>649.3</td><td>648.3</td><td>648.3</td><td></td><td>648.3</td><td>•</td><td>648.3</td><td>648.3</td><td>64H.3</td><td>648.3</td></th<>	649.3	648.3	648.3		648.3	•	648.3	648.3	64H.3	648.3
648.6 648.7 648.7 648.4 648.9 648.9 649.0 649.8 649.8 649.8 649.8 649.8 649.8 649.8 649.8 650.2 650.2 650.2 650.2 650.2 650.2 650.2 650.2 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8 650.8	644.3	44B.4	4.8.4		648.4	•	4.8.4	648.5	648.5	54A.5
440.1         644.6         649.6         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         649.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8 <td< td=""><td>644.5</td><td>648.6</td><td>644.7</td><td></td><td>548.4</td><td>_</td><td>648.9</td><td>649.0</td><td>649.1</td><td>649.2</td></td<>	644.5	648.6	644.7		548.4	_	648.9	649.0	649.1	649.2
450.7         650.3         650.4         650.5         650.6         650.6         650.6         650.6         650.7         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.8         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3         650.3 <th< td=""><td>646.3</td><td>449.3</td><td>4.4.4</td><td></td><td>9.649</td><td>_</td><td>8.649</td><td>649.8</td><td>6.649</td><td>650.0</td></th<>	646.3	449.3	4.4.4		9.649	_	8.649	649.8	6.649	650.0
K51.0         651.1         651.3         651.3         651.4         651.6         652.1         652.1         652.1         652.1         652.2         652.2         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3         652.3 <th< td=""><td>1.659</td><td>450.2</td><td>659.3</td><td></td><td>4.059</td><td>_</td><td>650.6</td><td>650.7</td><td>6.50.8</td><td>620.9</td></th<>	1.659	450.2	659.3		4.059	_	650.6	650.7	6.50.8	620.9
451.4         651.9         652.0         652.1         652.2         652.3         652.3           457.4         652.4         652.9         652.9         653.1         652.3         652.3           453.4         653.4         653.4         653.1         653.1         653.1         653.1           454.4         654.6         654.8         655.2         653.1         653.1         653.1           454.4         654.6         654.8         657.4         655.1         653.1         653.1           454.1         654.2         658.3         657.4         658.7         657.8         657.8           458.1         658.1         658.3         658.3         658.3         659.8         659.8           458.4         658.4         658.4         658.9         659.8         659.8         659.8           458.7         658.4         658.3         658.9         659.8         659.8         659.8           458.7         658.4         658.9         658.9         658.9         658.9         659.8           458.7         658.1         658.9         658.9         658.9         658.9         658.9           458.7         658.1         <	6.759	451.0	651.1		651.3	_	651.4	651.5	651.6	651.7
K52.4         K52.6         K52.8         K52.9         K52.9         K52.9         K53.1         K53.4         K53.4         K53.4         K53.4         K53.4         K53.4         K53.4         K53.7         K53.9         K53.7         K53.9         K53.7         K53.9         K53.9 <th< td=""><td>1.159</td><td>451.4</td><td>651.9</td><td></td><td>652.0</td><td></td><td>652.2</td><td>652.3</td><td>652.3</td><td>652.4</td></th<>	1.159	451.4	651.9		652.0		652.2	652.3	652.3	652.4
453.1         453.4         653.5         653.6         653.7         653.9           454.4         654.8         655.0         655.7         655.7         655.9           454.4         654.8         655.1         655.7         655.9         655.9           454.4         658.1         658.4         658.4         658.7         655.9           458.1         658.5         658.6         658.7         658.9         659.8           458.4         658.4         658.9         659.8         659.8         659.8           458.7         658.5         658.9         659.8         659.8         659.8           458.7         658.5         658.9         659.8         659.8         659.8           458.7         658.5         658.9         659.8         659.8         659.8           458.7         658.9         658.9         658.8         658.8         658.8           458.7         658.9         658.9         658.8         658.8         658.8           458.7         658.9         658.9         658.8         658.8         658.8           458.9         658.9         658.9         658.8         658.8         658.8	652.5	4.5.5	652.6		652.8		452.9	653.0	653.1	653,1
454.4 654.6 654.8 655.0 655.2 655.7 655.7 655.9 655.4 654.8 656.0 657.4 657.4 657.4 657.8 657.4 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 657.8 655.1 657.1 657.8 655.1 655.1 656.1 656.1 656.1 656.1 656.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.1 655.2 655.2 655.2	653.2	653,1	653.4		657.5		653.6	653.7	653.9	454.0
454.5         455.9         457.0         457.4         457.5         457.4         457.5         457.4         457.5         457.7         457.8         457.7         457.8         458.5         458.5         458.5         458.5         458.5         458.5         458.5         458.5         458.5         458.5         458.5         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.6         458.7         458.7         458.7         458.7         458.7         458.0         458.7         458.7         458.7         458.7         458.7         458.7         458.7         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8         458.8 <th< td=""><td>654.2</td><td>454.4</td><td>9.459</td><td></td><td>655.0</td><td></td><td>6.55.5</td><td>655.7</td><td>655.9</td><td>656.1</td></th<>	654.2	454.4	9.459		655.0		6.55.5	655.7	655.9	656.1
458.1         658.2         658.3         658.3         658.4         658.4         658.9         658.9           458.4         658.4         658.4         658.9         659.7           450.3         660.4         660.4         660.4         658.9         659.9           450.3         650.4         650.4         660.4         650.0         659.9           450.3         658.4         658.9         658.9         659.8         659.8           458.4         658.4         658.9         658.9         658.9         659.8           458.7         658.1         658.9         658.9         658.9         658.9           458.7         657.9         658.9         658.4         658.4         658.4           458.7         657.9         657.9         658.4         658.4         658.4           458.4         656.1         656.1         656.1         656.1         656.1           658.1         656.1         656.1         656.0         656.0         656.0           658.9         655.9         655.8         655.8         655.8         655.8           655.1         655.1         655.8         655.8         655.8         6	4.554	454.5	655.8		657.2		657.5	657.7	657.A	6.259
658.6         658.6         658.7         658.8         659.9         659.7           660.4         660.4         660.4         660.2         660.4         659.9         659.8           459.3         660.4         660.4         660.2         660.4         659.9         659.8           459.3         650.4         660.4         660.2         660.2         660.9         659.8           459.3         658.4         650.9         650.8         659.8         659.8         659.8           458.7         658.4         658.9         658.4         658.4         658.4         658.8         658.8           458.7         658.7         656.9         656.9         656.1         656.1         656.1           458.9         656.1         656.1         656.1         656.1         656.0         656.0           658.9         655.9         655.8         655.8         655.8         655.8           655.7         655.7         655.8         655.8         655.8         655.8           655.6         655.8         655.8         655.8         655.8         655.8	658.0	454.1	654.2		658.3		658.4	658.5	654.5	65.A.6
KAN,2         660.4         KAO,5         660.4         660.2         660.0         659.8           A59.3         K59.1         K59.0         K58.9         K58.9         K58.9         K58.8         K58.7         K58.7         K58.7         K58.7         K58.7         K58.7         K58.7         K58.7         K58.7         K58.8         K55.8         K55	671.6	658.6	654.6		658.6		658.8	628.9	659.2	659.5
A59.1         A59.2         A59.1         A59.0         A58.9         A58.0         A58.9         A58.9         A58.9         A58.9         A58.9         A58.9         A58.9         A58.8         A58.8 <th< td=""><td>6.4.54</td><td>2.099</td><td>4.099</td><td></td><td>660.5</td><td></td><td>660.2</td><td>0.049</td><td>8.659</td><td>659.6</td></th<>	6.4.54	2.099	4.099		660.5		660.2	0.049	8.659	659.6
458.4         658.5         658.5         658.5         658.4         658.4         658.4           458.7         457.4         457.4         657.6         657.6         657.5           457.3         657.7         657.9         656.9         656.8         657.6           456.4         656.4         656.9         656.3         656.1         656.1           658.1         656.1         656.0         656.3         656.3         656.3           658.1         656.1         656.0         656.0         656.0           655.9         655.9         655.8         655.9         655.0           455.0         655.9         655.8         655.8         655.8           455.7         655.7         655.7         655.6         655.6           655.6         655.5         655.5         655.5         655.6	4.956	454.3	454.2		659.0		65A.9	458.8	6.58.8	658.7
KSR.2         KSR.1         KSR.3         KSR.4         KSR.5         KSR.5         KSR.5         KSR.7         KSR.8         KSR.8         KSR.7         KSR.8         KSR.8         KSR.7         KSR.9         KSR.9 <th< td=""><td>45A.7</td><td>55R.6</td><td>658.6</td><td></td><td>658.5</td><td></td><td>658.4</td><td>658.4</td><td>658.4</td><td>65.4.3</td></th<>	45A.7	55R.6	658.6		658.5		658.4	658.4	658.4	65.4.3
657.3 657.7 657.1 657.0 656.9 656.8 656.7 656.7 656.7 656.7 656.8 656.7 656.7 656.7 656.7 656.7 656.7 656.7 656.7 656.7 656.0 656.0 656.0 655.0 655.0 655.0 655.0 655.0 655.0 655.0 655.0 655.0 655.0 655.0 655.8 655.8 655.8 655.8 655.8 655.8 655.8 655.8 655.8 655.8 655.8 655.8	6.8.3	454.2	454.1		657.9		457.7	657.6	657.5	657.4
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654.1 656.1 656.1 656.0 656.0 656.0 656.0 656.0 656.0 655.0 655.4 655.4 655.4 655.4 655.4 655.6 655.6 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5 655.5	656.6	454.4	654.5		556.4		656.3	656.3	656.7	656.2
655.9 655.9 655.9 655.8 655.8 655.8 655.8 655.8 655.8 655.8 655.7 655.7 655.6 655.6 655.6 655.6 655.6	656.2	654.1	656.1		656.1		656.0	656.0	656.0	656.0
455.7 455.7 455.7 655.7 655.7 655.6 655.6 655.6 655.6 655.4	655.9	655.0	655.9		6.55.9		655.8	655.8	655.8	6.55.8
655.4 655.4 655.8 655.5 655.5 655.5	1.559	455.7	455.7		1.559		455.7	655.6	655.6	655.6
	9.559	455.4	655.6		655.5		655.5	655.5		

16.17 HOURS	
AT TIME	
1933.	
OUTFLOW IS	
PEAK	

101AL VOLUME 59747. 59747. 10.72. 277.32. 411. 508.	
72-HOUR 201. 10.72 272.32 411. 508.	
24-HOUR 207. 10.72 272.32 411. 508.	
6-HOUR 721. 20. 9.32. 236.62. 358.	
PEAK 1933. 55.	
CFS CAS INCHES AN AN AC-FT	

#### 133. MAXIMUM STORAGE =

#### END-OF-PERIOD HYDROGRAPH ORDINATES STATION OUTING. PLAN 1. PATIO 5 outFLow 0. 0. 0.

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 	ي ته	27.	30.		59.	243.	908.	1314	1804.	911.	689	320.	122	1221	. 18	78.			•	•	-	<b>.</b>		ง ค	้นก	12.	21.	30.	• •	58.	66	93	108.	3 0	131.	15	20	000	93.	40	78.	76.			å,	646.1	: :		
	, ,	26.	35.	e 0	55.	207.	79.	1097.	1976.	950.	708.	337.	194	• u		78.	75.		•	•	-	<b>.</b>	<u>.</u> ;	, e	•	11:	٠u2	29.	36.		57.	91.	107.	116	134.	115.	.01.		9 0	900	78.	77.	75.		ď.	248.1	:		
::::		25.	34.	• • • •	54.	177.	57.0°	961	2148.	266	724	354.	143	150	85.	78.	76.		•0	•		<b>.</b>	.;		; ;	10.	19.	28.	, de	5.	99	3	107.	<u> </u>	38.	2	2:	56		900	78.	.;	ė		ď.	244		ċ	
	m ;	 	*	* * *	53.	153.	534.		2299.	040	740.	370	- 207	000		79.	16.	نعا	,	•	-	<b>.</b>			;	<b>.</b>	18.	27.	37.	, v	6.5	A.	106.	111	140	117.	-11	106.		6.0	79.	77.	.2.		å.	244			•
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	€.	20.	31.	39.	52.	82.	369.	. 646	2332.	1256.	799.	523 <b>.</b>	• > C >	000		90.	.11.		•	•	•	-	<b>.</b>	•			15.	24.	* e	• • •	62.	76.	102.		141	121.	112.	• 90	96.	81.	79.	77.	. 6.			248	_ ``		•
	~	£ 0.	30.	0 u	51.	75.	139.		2142	1344.	823.	577.	.58.		87.	ď	77.		•	c	ċ	-	- 1	2		ç	÷.	54.	er.	5 C	.19	75	100.		138.	5	113.		96.	£	79.	77.	. 4.		÷	549.1	•		٠.
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648.2	648.2	648.2	648.3	648.3	648.3	648.3	648.3	648.3	648.
648.3	648.3	648.3	648.3	648.4	648.4	648.4	648.4	4.8.9	648.4
649.4	4.44	648.4	648.5	648.5	648.5	646.5	648.6	648.6	648.
648.7	648.8	648.8	648.9	649.0	649.1	649.2	649.3	9.649	649
9.649	440.7	649.A	6.649	650.0	650.1	650.2	650.3	<b>650.4</b>	650.
650.6	450.7	650.A	6.059	651.0	651.1	651.2	651.3	421.4	651.
651.6	451.7	6.159	651.9	652.0	657.1	652.2	652.3	452.4	655.
652.5	655.6	652.7	652.4	6.259	653.0	453.1	653.2	653.3	653
653.5	451.6	453.7	653.7	653.A	623.9	654.0	654.1	654.2	654
654.4	4.454	654.5	654.6	654.7	6.454	6.459	655.0	655.2	655
655.5	455.7	654.0	656.2	656.4	656.7	656.9	657.1	657.3	657.
457.7	657.A	658.0	658.1	658.2	654.3	658.4	658.5	658.5	658
654.6	65A.6	653.6	658.7	654.7	658.4	658.8	658.A	658.9	654.
4.54.9	454.9	659.0	654.0	659.0	659.0	659.1	659.3	9.659	660.
669.4	A.00.	661.1	661.2	661.2	661.0	640.B	4.094	660.3	560.
6.659	659.7	654.5	4.654	654.3	659.2	659.2	659.1	1.659	653
654.0	6.954	654.9	65H.A	659.8	65R.7	458.7	654.7	9.859	658
654.5	458.4	65H.3	654.2	658.1	658.0	6.1.9	657.A	657.7	657.
657.5	4.754	657.3	657.3	657.2	657.1	657.0	657.0	6.959	656.
555.B	456.7	654.6	656.4	656.5	656.5	656.4	4.959	656.4	656.
655.3	656.3	654.2	656.2	656.2	656.2	656.1	656.1	656.1	656
654.1	6.984	456.0	656.0	654.0	654.0	656.0	656.0	6.55.9	655
654.9	6.554	6.55.9	645.9	655.9	6.559	455.8	455.A	655.B	655
655.8	6.55 A	655.A	A55. R	655.8	ASS. A	455.7	655.7		

HOLIAS
16.17
TIME
1
2414.
18
OUTFLOW
PEAK

TOTAL VOLUME	74936.	13.81	350.66 530.	654.
72-HOUR	267.	13.81	350.66	654.
24-HOUR	267. B.	13.81	350.66	454.
6-HOUR	931.	12,02	305.43	569.
PEAK	2414.	•		
	CFS CFS	INCHES	AC-FT	THOUS CO M

### MAXIMUM STORAGE = 143.

STATION OUTING. PLAN 1. RATIO 6
END-DF-PERIOD HYDROGRAPH ORDINATES

	•	ė	•		-	-	~	5	20.	38.	51.	100	234.	321.	475.	1076.	1363.
OUTFLOW		•	•	<b>:</b>	<b>:</b>	<b>:</b> :	~	÷	18.	37.	50.	**	224.	316.	413.	1038.	1346.
	•	•	6	٦.	-:	.:	۶.	е	16.	35.	64	78.	209.	310.	368.	995.	1329.
	•	•	•	;	-:	-:	۶.	М		34.	48.	74.	193.	304.	354.	945.	130H.
																	1284.
	•			-:	<b>:</b>	<b>:</b>	؞	å	10.	30.	45.	<b>64.</b>	169.	289.	341.	825.	1256.
	ė	•	•	-	-:	-	۶.	2.	•	2Α.	;	59.	157.	201.	338.	762.	1223.
	•	•	•	ċ	-	-	~	٠.	9	26.	43.	55.	144.	271.	334.	693.	1184.
	•	•	•	•	<b>:</b>	-	ζ.	۲.	۲.	25.	42.	53.	139.	261.	330.	619.	1152.
	•	•	•	•	:	-	-	۲.	į	23.	<b>*</b> U <b>*</b>	52.	115.	250.	376.	545.	.,,,,,,

1675		10	1768.	1242	5.5	243.	172.	148.	135.	124.			ď	<b>.</b>	•	: .	• •	, ,	•	<b>:</b> :	::	•	• 7	-	• •	93.	•	. 04.	. 8.	123.	129.	157.	159.	130.	121.	104.	٠٢6	8A.	85.	•	<b>A</b> 3.			1 949	648.7	648.2	648.3	64A.4	64R.5	64A.7	2.649	650.8	652.6	654.5	656.2	6.27.3	1.10	658.2	654.3		1.000	
2	9			1343	50								9			• .		• •	;	• •	9 6	• • • •	•			92.	98	103.	117.	123.	128.	146.	166.	132.	123.	105.	94.	₩.	86.	* 6'	83.						å	÷	÷	÷	÷	ċ	å.	٠.	٠.	٠.	٠,	658.1	•	: .	: -	•
1621	7 2 2	1951	220	1385.	560	271.	179.	151.	137.	129.	125.		ć	: -	•	: ,	• •	• •	: .	ċ	;		, ,		:		.86	102.	116.	122.	127.	138.	172.	133.	123.	106.	95.	A9.	8h.		A3.	63.		448.1	648	4.8.2	B.	648.4	648.5	648.7	649.0	650.5	652.3	654.1	6.55	657.1	2.700	6.58.5	7044	00400	000	• • • • • • • • • • • • • • • • • • • •
88	1925	201	2009.	1416.	623.	786.	183.	153.	138.	130	155.				-		نہ ڈ	•	;	•	•	• • • •		n	•	• 6	97.	101	115.	122.	127.	133.	179.	135.	124.	108.	96	.60	gę.		83.	63.														657.0		657.9	4.59.6	-	2004	-
1549.	1794.	9	2108.	1447	692	303.	197.	156.	139.	130.	126.			: -	: _:					n a	•	• •		•	÷ ;			100.	1.4.	121.	176.	131.	184.	137.	124.	110.	97.	٠،6	B.,	45.	<b>.</b>	A3.		649		648.2											:	627.9	, 0	,	: .	•
1509.	1743.	4783	2227	14A2.	764.	320.	193.	154.	140.	131.	126.	STOBARE	•		: -				•	r. r	• •	• (		'n	- ;		, 9¢	100	113.	121.	125,	130.	148.	139.	125.	112.	9 <b>4</b> •	6،	A7.	85.	8	83.	CTAGE	2	648.1	648.2	648.2	648.3	648.5	648.6	648.9	650.0	651.7	653.5	655,3	656.8	0,70	657.8	650 A	410	640	•
1470.	1726.	4811	2370.	1526	H52.	336.	201.	160.	.25.	132.	126.		0	ė	-	: .			÷ ų	, ,			200	e c	•	989	96	001	:::	120.	125.	129.	169.	142.	126.	114.	104.	6	87.	٠ د	æ	83.		648.1	648.1	648.2	648.2	648.3	4.8.4	644.6	648.8	54.0	651.5	653.4	655.2	656.7	د. ۱۲۵	657.A	000 400	410	F 6 6 4	
1435.	1718.	4639	2544.	1574.	964	353.	210.	163.	* * * * * * * * * * * * * * * * * * *	25.	127.		0		-	: _			7 4		:	• •	•		• •	82.	5.6	• 66	110.	120.	124.	129.	185.	145.	127.	116.	101.	91.	R7.	45.	34.	83.		648.1	548.1	64B.2	648.2	648.3	648.4	448.6	648.8	649.6	651.3	453.2	455.0	656.6	6.700	657.8	6.00.4		200	
1405	1700	270	2754	1635.	1090	348.	229.	144.	- 4 4 F	134.	127.		ď		: _:	: _			•	• •	• ;		:			a	96	•	108.	119.	174.	129.	178.	149.	12%.	114.	102.	92.	е7.		A .	A3.		648.1	648.1	54E.V	548.2	648.3	44B.4	648.5	A. B.	449.5	651.2	453.0	654.R	656.4	40,000	4.7.4 4.00	r. 504			•
1381.	1695.	3742.	3002	1699.	1197.	*04.	731.	200	•	. 46.	164.		0	•	-				: ,	• •	֓֞֞֜֜֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		• • • •		• :	60	46	3	ş	Ξ.	123.	129.	168.	š	129.	120.	5	93.	æ	٠ ٢	:	<b>.</b> 3.		64B.1	646.1	64R.2	648.2	648.3	648.4	648.6	643.8	4.6	651.0	652.8	654.6	655.3	2.4.0	657.8	459.3	46.0	660	

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.02	-02	-05	0				¥0.	- 02	20.	- 05	.0.	- 02	.02	-02	-02	20.	20,		-05	33.80	UME	15.	25.	31.54	.18	81.	4418.		3711 100	1 0					442			1		,	6.31		716.		•			E E	56005.	.418.	9.46
270	27.1	272	273	7.2		613	5	277	278	279	280	283	282	233	284	285	286	786	288	SUM	TOTAL VOLUME	520015	147	. F	603	35	\$	-	TOTAL VOI		- -		9		*		v	TOTAL VALUE	10400	2		140	-	- •	c	•		TOTAL VOLUME	1560	:	•
22,30	22.35	22.40	22.45	200	9 4 6 6	66.00	20.00	63.65	23.10	23,15	23,20	23.25	23,30	23,35	23.40	23.45	23.50	23.55	0.00		12-HOUR I			31.54	1,18	101.	4418.		72-HOUR T			51.15	21.0	. W. C.	442.			72-MOUR T		10.	31	160.24	116.		•					.5.	9.46
1.01	1:07	1.01	100				10:1	1.01	1.01	 	1.01	1.01	<u> </u>	10.1	1.01	1.01	10.1	-	1.02		12-1							PLAN	72=4		•						~ V V	72-4					•			D AN		72			
055.		051.	•	06.7	• 650	•	• 11.5	•	077.	0.79	082.	044.	046.	ď	.040	. 650	950	046.	0.48.		24-HOUR	1805.	51.	31.54	801.18	3591.	4414.	AT STAINFLOW FOR PLAN 1. RTIO	24-HOUS	1.4.1	,	3.15	80.12	25.8	442.		AI SIAINFLOW FOR PLAN I. MILO	24-4018	361.	10.	6.31	160.24	716.	400	•	OTTO - C NE 19 BOT BO BUILD TO BE BE SEEN TO STATE OF THE		74-HOUR	542	15.	9.46
	_	~		• -		•	-	~	_	_		_	_			-	-	-			6-H0UR	5741.	163.	25.07	636.43	2847.	3511.	AT STAIN	GUOH-Y	57A	-	2.51	63.68	285	351.		AI SIAIN	4-HOLLD	1148.	33.	5.01	127.37	569	702	•	AT STAIN	,	6-H0UR	1722.	40	7.52
	6	٥.	6.	5	•		-	0		0	5	ē.	6.	•	٥.	.0	6		.00		¥																									NO VO					
10.	.07	.07	.07					.0.	20.	.07	20.	.07	.07	.07	.07	10.	. 07	. 0.	-0.		PEAK	16458	466					HYDROGRAPH	PFA	1666	7.						HOROGRAPH	DFA	3202	6						HVDROG		PEA	4937.	140	
40.	-07	.07	.07	2				10.	. 0 •	.0.	.01	.07	.07	20.	. 07	.07	.07	200	.07			CFS	CMS	INCHES	ī	AC-FT	¥ C.			7	, v	TACHES	3	16-54					CFS	CAS	INCHES	ĭ	AC-FT		3				CFS	Ç	INCHES
126	127	12A	129	2			7.	7	7	135	36	137	134	139	140	-	142	1	:								<b>1</b> H0US								THOUS						•			THOUSE							•
10.30	10.35	10.40	19.45	10.50			2	50.11	01.1	c:::	2.	11.25	11.30	11.35	11.40	11.45	11.50	11.55	12.00																																
10.1	~ ·	~ °	1.1	100				10.			7	1.,1	٦. ت	10.1	1.01	10.1	1.01		1.01																																

TOTAL VOLUME 156005. 4418. 9.46 240.35

24-HOUR 542. 15. 9.46 240.35

6-HOUR 1722. 49. 7.52 191.05

CFS CMS · INCHES

THOUS CU H		1053.	1325.	1325.	1325.
	нувробрарн	AT STAIN	IFLOW FOR	AT STAINFLOW FOR PLAN 1. RTIO 4	<b>4</b> 01
	PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL VOLUME
CFS	6583.	2296.	722.	722.	20A006.
SAC	186.	65.	20.	20.	5890.
INCHES		10.03	12,42	12.62	12.62
I		254.73	320.47	320.47	320.47
AC-F		1139.	1433.	1433.	1433
THOUS CO M		1405.	1767.	1767.	1767
	HYDROGRAPH	AT STAIN	IFLOW FOR	HYDROGRAPH AT STAINFLOW FOR PLAN 1. RTIO 5	10 S
	PEAK	4-HOUR	24-HOUR	72-H0UR	TOTAL VOLUME
CFS	8229.	2970.	103.	903	260008.
CMS	233.	81.	26.	26.	7363.
INCHES		12.54	15.77	15.77	15.77
1		318.42	400.59	400,59	400.59
AC-FT		1423.	1791.	1791.	1791.
THOUS CU M		1756.	2209.	2209.	5509
	HYDROGRAPH	AT STAIN	IFLOW FOR	MYDROGRAPH AT STAINFLOW FOR PLAN 1. RTIO 6	10 6
	PEAK	6-H0UR	24-HOUR	72-H0UR	TOTAL VOLUME
CFS	16458.	5741.	1906.	1806.	520015.
C#S	466.	163.	51.	51.	14725
INCHES		25.07	31.54	31.54	31.5
Z		636.83	901.18	801.18	801.19
AC-FT		2847.	3581.	3541.	3591
THOUS CU M		1136	74.16	0111	9111

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	COMPINE HYDROGRAPHS
	E#00

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LAKES MARIAW, SUGARHOLLOW, ROBINHOOD, AND SHERWOOD HYDRO
15TAQ ICOMP IECON ITAPE JPLI JPRI INAME 1STAGE 1AUTO
4 -0 -0 1 3 1 -0 -0

RTIO 1	TOTAL VOLUME 84284. 2367. 60.29 580. 716.
PLAN 1	72-HOUR 203. 7.37 60.29 580.
AT	24-HOUR 293. 7.37 60.29 580. 716.
	6-HOUR 792. 782. 1.41. 40.79 993.
OF 4 HYUROGRAPHS	PEAK 1814. 51.
NOS	CFS CONS TNCHES HE AC-FT

RT10 2	107AL VOLUME 192930 • 5463 • 5463 • 5.43 13A • 00 1329 • 1639 •	RTIO 3 107AL VOLUME 302953. 8.53 216.69 2046. 2574.	RTIO 4 TOTAL VOLUME 4134.7. 11.64 295.70 295.70 295.70	ATIO 5 14847. 14.76 375.02 3611. 4454.	7
PLAN 1	72-HOUR 64.00 134.00 1329.	PLAN 1 72-HOUR 1052. 30. 8.53 216.69 2046. 2574.	PLAN 1 72-HDUR 1435. 11.64 295.70 285.70 3512.	72-HOUR 1820. 52. 14.76 375.02 3511. 4454.	72-H0 375- 10 30- 777- 743-
AT	24-HOUR 670. 19. 5.43 138.00 1329. 1539.	24-HOUR 1052. 30. 8.53 216.69 2086.	AT 24-HDUR 1435- 11.64- 295-70 2847- 3512-	24-HOUR 1820. 52. 14.76 375.02 3411. 4454.	
HYDROGRAPHS A	6-H0U9 2049. 58. 6.15 105.54 1016.	HYDROGRAPHS A K 6-HOUR 3356. 95. 5.68 172.85 1664.	HYDROGRAPHS . 6-MOUR . 657 9-48 . 58 . 240. 58 . 285 2859.	HYDROGRAPHS  K 6-HOUR  5990.  170.  170.  308.51	HYDROGRAPHS  K A-HOUR  12236.  347.  24.81  630.97
OF 4 HYDR	5303. 150.	0f 4 8 P E 4 250	0F 4 11341 335	0F 4 1 16742 11742	OF 4 29409 833
NUS	CFS CHS TNCHES AC-FT THOUS CU M	CFS CMS CMS INCHES AM AC-FT THOUS CU W	SUM CFS CFS CMS INCHES ACFT THOUS CU M	CFS CFS CFS TNCFES THOUS CU H	CFS CFS CFS TNCHTS TNCHTS TH ATH AC-FT

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		RESER	RESERVOIR ROUTING FOR LAKE SHERWOOD ISTAG ICOMP IECON ITAPI	TING FO	4 LAKE SHI	SHERWO	WOOD ITAPE	JPLY	JPRT	INAME	151	IAUTO		
			OUTING	~	-	ROUTING DATA	0-0 0A7A	N	~	-	Ŷ			
		0.05	CL055	AVG -0.00		S: ~	SAME 1	1001	P N O		LSTR -0			
			NSTPS	NSTDL -0		LAG AV	AMSKK -0.000	× 00 - 0-	1SK -0.000	STORA -623.	ISPRAT			
STAGE 62	622.8 627.5	62.5	623.0 628.0	623.5 628.5	33	624.0 629.0	624.5 629.5	ພໍ້	625.0	625.5 630.5	in in	626.0	626.5 631.5	627.0
FLOW	522.	ž	748.	13.	2	35. 1242.	64.	÷ 6.	98. 2645.	13	135. 6298.	183.	252. 8929.	376.
CAPACITY=	6969	.,,	28. 775.	100. B54.	172, 934,		244.	200	318.	392. 1178.	466.	542.	619.	
ELEVATIONS	623. 627.	66	623. 628.	623.	624.	• •	624.	9.9	625. 630.	625. 630.	626. 631.	676.	627. 632.	
		, , , , , , , , , , , , , , , , , , ,	CREL SP 622.8 -	SPW10 -0.9	C00#	EXPE -0.0	ELEVL -0.0		COAL C/	CAREA E	Expt -0.0			

DAM DATA
TOPEL COOD EXPD DAMMID
629.6 -0.0 -0.0 -0.
STATION OUTING, PLAN 1. RATIO 1

## END-OF-PERIOD HYDROGRAPH ORDINATES

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	•	· e			•	•	•	•		ė		: _	,	; ;	8		11.	19.	30.	<b>4</b> 8.	90.	117.	143.	163.	171.	176.	179.	181.	184.	,
	•	•			; ,	•	•	•			-	: _		'n	'n		11.	17.	29.	45.	87.	115.	141.	161.	171.	175.	179.	181.	183.	184.
	•	•	•	<b>.</b>		;	•	•		•	-	-		'n	ທ	7.	10.	16.	27.	*5*	94.	112.	137.	160.	170.	175.	178.	181.	183.	. A.
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OUTFLO	•	ď				•	ċ	•	•	•	-	: _:	5.	п	'n	÷	•	15.	25.	38.	76.	107.	132.	157.	149.	174.	178.	180.	143.	) n5.
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	•				-	-		'n	æ				3 0	<b>&gt;</b> •	• 000	95.	8	~	155.	204.	302.	357.	90	435.	449.	455	460.	464	467	•			622.8	622.8	622.8	622.8	652.8	6.22.9	622.8	6559	6559	6559	423.n	623.0	1.520	255	7.524	423.6	9.00	624.2	654.9	625.3	625.6	625.A	6.55.9	675.9	626.0	626.0	675.0	
	ě		•		-	: -			,,	_					.64	00	83	77.	151.	196.	296.	352.	401.	433	*	455	460.	494	467	* 4 V	•		622,8	625.8	622.8	422.8	622.A	2.	6.229	25.	22.	422.9	655.9	5	::	;;	7	5	֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	24.	7	25	625.6	625.8	6529	25.	626.0	50.	٠,	0.0%0
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STOOLGE							- (						: ;	<b>.</b>	• • • •	57.	75.	104.	139.	190.	271.	336.	397.	426.	445	453	4.8	463.	466	9	•	STAGE	_	622.₽	622.8	622.8	622.8	622.B	652.8	622.8	622.8	6559	6559	623.0	1,520	1.00	200	623.5	623.8	624.1	624.7	625.1	625.5	625.7	6.55.9	6.55.9	625.9	626.0	626.0	0.070
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	ć	•	•	•	• •	• .	•			٠.	3 P	٠ ٧	n .	•	•	•	70.	97.	131.	72	0	25	377.	421.	3		5	462.	465		•		22.	622.8	25.	22.	652.8	22.	25.	22.	25.	25.	25.	623.0	;	;		A 23.45		24.	2	25	25.	25.	.5.	52	3	\$	624.0	0.020
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:	ć				• -	• .				•			į	• •	*S	52.	65.	91.	124.	163.	225	314.	367	*14	433	.054	456.	461	<b>*</b> • • • • • • • • • • • • • • • • • • •	4	•		625.8	627.8	62%,8	622.8	622.8	622.8	622.8	622.B	622.8	6529	655.9	623.0	0530	673.1	200	623.4	623.7	623.9	624.4	625.0	625.3	9.529	625.8	6529	6,52,9	626.0	476.0	0.00

STATION OUTING. PLAN 1. PATIO 2

END-OF-PERIOD HYDROGRAPH ORDINATES

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763.	760.	758.	755.	752.	749.	7.47	744.	742.	-
737.	734.	732.	730.	727.	725.	123.	721.		
				STAGE					
627.8	622.R	622.8		622.8	_	422.8	622.8	622.8	ë
625.8	455.4	422.A		672.A	_	422.8	622.B	622.A	£
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622.B	622.A	427.A		627.B	•	622.8	622.8	622.R	¢
622, B	622.A	642.B		622.R	•	622.8	622.A	622.8	¢
622.8	4.22.A	622.A		622.8	•	622.8	622.A	622.8	Ġ
622.8	627.A	622.B		622.8	•	622.8	622.8	622.8	ف
6.449	6529	6.224		655.0	_	655.9	6559	655.9	Ċ
657.9	6559	655.9		623.0	•	623.0	623.0	623.0	Ģ
623.0	423.0	623.0		623.1	_	623.1	623.1	623.1	ě
623.1	423.1	423.2		623.2	•	623.2	423.2	673.2	ž
623.3	423.3	673.3		623,3	•	623.3	4529	453.4	623.4
623.4	453.4	623.4		623,5	_	6.23.5	623.5	623.5	Š
623.5	623.6	623.6		623.6	•	623.6	623.6	623.7	č
623.7	423.7	623.B		623,8	_	423.9	653.9	624.0	č
624.1	624.1	624.1		624,2	•	624.3	624.3	4.429	č
624.5	454.5	9.429		624,7	•	6.459	624.8	654.9	ë
625.0	525.n	625.1		625,2	~	625.3	455.4	625.6	č
655.4	424.1	4.929		626,B	•	627.2	4.7.4	627.5	ě
8.759	427.9	624.0		62A.2	•	4.864	629.5	624.5	ž
624.6	52A.7	424.7		628,8	•	428.9	6.8.9	62H-9	ž
629.0	429.0	629.0		629.0	•	678.9	428.9	658.9	č
6.829	478.9	628.A		628,8	•	428.7	428.7	628.7	ટ
624.6	428.4	624.6		62A.5	•	6.85.5	428.4	624.4	È
628.4	42P.3	628.3		629.3	•	428.2	624.2	628.2	ž
628.1	628.1	628.1		628.A	•	628.0	62A.9	624.0	ě
627.9	627.0	657.9	6.7.5	657.9	627.8	627.8	627.A	627.8	è

PEAK OUTFLOW IS 1229, AT TIME 18.58 HOURS

	PEAK	6-HOUR	24-MOUR	72-HOUR	TOTAL VOLUME
CFS	1229.	992	307.	307	84298
SAS	35.	28.	•	6	2500.
INCHES		2.01	2.49	2.49	64.4
ĭ		51.07	63.16	63.16	63.16
AC-FT		492.	608.	4.08.	6AB.
5 CC 11		607.	750.	750.	750.

MAXIMUM STORAGE = 93

STATION GUTING. PLAN 1. RATIO 3

ö			•				-:	-:	;	œ	12.	00.	28.	36	65.	106.	187.	542	980	4032.	3210.	2040.	367	258	40	962	841.			•	-	:	~	m •	•	ġ		, E	 93.	120.	149.	181.	246.	334.	471.	686.	
•	•	•	•	•	•	•	-:	<b>:</b>	*	•	15.		27.	37.	62,	101	174.	**1	2611.	4.085.	3295.	2147.	1377.	1269.	1119.	975	852	751.		•	:	-:	~	m.	•	• •	• 6		· •	118.	146.	177.	239.	324.	453.	653.	
•		•	:	•	•	:	<b>:</b>	<u>.</u>		7.			56.	35.	.65	96	164.	391.	2143.	4121.	3377.	2296.	1388.	1280.	1135.	989	863.	160.		•	-	-	તં	m -	<b>:</b> .	• •		9.0	 97.	115.	143.	173.	231.	315.	437.	627.	
•	•	•			•			-	۳.	7.	_		56.		26.		153.	353.	1563.	4138.	3460.	5404.	1403.	1291	1151.	1003	875.	769.	Įų.	•	1.	-	2	, V	• •	n a	•	37.		2	=	176.	224.	305.	421.	ø	
OUTFLOW 0.	•		•	• 0	ė	•	ė	:	,,,,	2	-		r.			98	143.	320.	332	131		2512.	1488.	1302.	1167.	1016.	887.	179.	STORAGE			-	۶.	å.	• :	ŗ		ď	 . 0	109.	137.	167.	217.	296.	404.	584.	
:	•	•	•	•	•	•	•	-:	,			<u>.</u>				96	134.	26.7	234	195	3634.	2614.	57A	1312.	1183.	1031.	٠ ٠ ٠	769.		ė	•	-	ċ	~•	ř.	'n	: ;			106.	135.	164.	210.	287.	391.	564.	•
•	•		ċ	•	•		•							2	4	0.00	124.	25h.	4.20	020	3722.	2748.	1672.	32.	1200.	1045	911.	.667		•	•	;	:	n, i	n° 1	, ,	: :		 77.	3	32	161.	203.	279.	378.	545	
•	•	•	•	<u>.</u>	ċ	ċ	•		`~	ی	•	• •		· -	, v	76.	122.	238	907	3898.	3494.	2881.	1770.	1334.	1216.	1050	923.	608		•	•	<i>-</i> :	:	∾ ′	m .	ŗ,	:;	. 00	74.	=	2	ISA.	197.	270.	346.	526.	
ė	•	•	•	•	ė.	ċ	•	-	ζ.	,	. ,	· -	. ~			72.		20.	•	13.	91.	17.		٠. د د	33.	:		٠٠.		:	ė	-	<u>:</u>	٠.	• ,	ŗ,	: .			99.	۲.	55.	91.	52.	355.	٠.	

1150.	1154.	1150.	1146.	1141.	1137.	1133.	1129.	1125.	1170.
1114.	1108.	1102.	1095.	1084.	1091.	1074.	1066.	1059.	1052.
1046.	1039	1033.	1026.	1021.	1015.	1010.	1004.	666	E. 00
997.	942	976.	971.	965.	959	954.	840	942	937.
931.	924.	920.	915.	910	. 100	899.	894	849.	88.
879.	974.	B70.	865.	660.	856.	. 1821	847.	843.	839.
835.	. I. O	827.	H23.		и)5.	412.	808	A04.	401.
704.	704.	791.	744.	784.	782.	.414	176.		
				STAGE	***				
622.8	622.A	622.8	622.A	622.A	•	622.8	622.8	622.A	622.8
627.8	4525.4	627.A		655.8	•	622.8	6.25.8	622.A	422.A
627.8	422.A	622.A		622.8	•	422.8	622.A	4.22.4	622.B
622.8	422.8	427.B		622.8	•	622.4	622.R	622.R	622.A
8.7.4	422.A	625.8		622.A	•	622.B	672.A	622.A	822.A
627.B	A22.A	422.9		6529	_	6.23.8	622.B	622.A	672°B
622.R	A22.A	622.A		622.8	•	622.8	622.B	627.A	622.B
6.55.8	627.A	622.8		655.9	•	455.4	6.22.9	655.9	6.22.9
6529	422.9	6.52.4		6.59	•	422.9	623.0	623.0	623.0
623.0	423.0	623.0		623.0	•	623.1	623.1	623.1	623,1
623.1	6.53	423.2		623.2	•	623.2	621,3	623.3	643.3
6,83,3	6.1.3	623.3		623.4	•	453.4	623.4	623.5	6,3.5
623.5	623.5	473.5		623.6	•	623.6	623.6	623.6	523.7
623.7	623.7	423.7		623.A	•	623.8	623.A	623.8	423.9
653.6	653.9	453.9		624.0	•	624.0	424.0	624.1	624.1
624.1	424.2	424.2		624.3	•	4.429	624.5	624.5	624.6
9.429	424.7	624.7		654.9	•	625.0	625.0	625.1	425.2
625.2	K.25.3	455.4		625.6	•	6.55.8	6.529	626.0	626.1
6,454	454.4	654.5		626.A	•	427.1	627.2	627.4	K27.7
0.429	624.3	424.7		629.3	•	6.29.8	630.0	630.1	630.2
634,3	430.4	4.30.4		630.4	•	630.4	430.4	630.4	4.019
4.064	430.4	630.3		630.3	•	630.2	630.2	630.2	630.1
630.1	430.1	630.0		659.4	v	6.624	629.8	629.A	629.7
624.7	9.629	624.6		659.5	•	659.5	4.629	₹.629	4.669
6.629	6.65A	6.629		629.2	•	4.629	1.629	629.1	629.0
0.669	658.9	6.45.4		62A.B	•	6.8.4	678.A	624.7	62A.7
624.7	428.6	624.6		62A.5	•	6,8.5	628.5	628.4	57A.4
4.829	424.4	624.3		624.3	•	6.88.2	62A.2	624.2	52A.2
624.1	624.1	626.1		628.1	628.0	6.28.0	628.0		

PEAK GUTFLOW IS 4138, AT TIME 17.17 HOURS

TOTAL VOLUME 190341. 5.30. 5.36 136.14
72-HOUR 661. 19. 5.36 136.14 1311.
24-HOUR 661: 19: 5.36 136:14 1311: 1617.
6-HOUR 2229. 63. 4.52 114.78 1105.
PEAK 4138. 117.
CFS CMS INCHES MN AC-FT TMDUS CU M

MAKIMUM STORAGE = 1171.

STATION OUTING, PLAN 1, RATIO 4 END-OF-PERIOD HYDROGRAPH ORDINATES

	ó	•	•	•	•	•	•	-	_		÷,	:	12.	23.	32.	46.	,			·		1347	A070.	578A.	4132	2434	1303	0000			1019.	896.			ċ	-:	~	, ,			ž				124	143	• •	24.2	335			:	1014.	1317.	1237.	1170.	1083.
	0			;	•	•		•	_		• •	:	12.	<b>5</b> 0.	31.	*	7			-	200	1297.	R122.	6002.	4252	2567	1666		000	• • • • • • • • • • • • • • • • • • • •	1031.	907.			•					<b>1</b>				9	ינכו			9.0	200	,,,,	017		962	13)4.	1245.	1176.	1001
	ė		•		•	•	•					ċ	=	.61	30.	43.	9	· .		• • • • • • • • • • • • • • • • • • • •	204	1501	A046,	6214.	4380.	2716.	16.35	010		1184	1044.	919.	A] 4.		•	-:	2			<b>.</b>	2			4		1 1 1		2.1.	12.			• • • • •	921.	1316.	1253.	1182.	1100.
	•			:	•	•	•	•	-		•	3	:	18.	29.	<b>4</b> ].	57.5	6		000	• 1	1944.	7794.	6435.	4520.	2497.	1631		1 36 4		1057.	431.	A23.		•	-	-			•	=	27.	2	82	1.6.	15.		226.	305	431.			. HE/	906	1262.	.187	1109.
				•			•		-			'n	=	1.	28.	•0•					37.5	1014.	132%	. [649	4668.	3085.	1734.			121	1071.	943.	833,	لوا	•	١.			้นก		-			9				227	202				# 70	1296	1276.	1193.	
10.13(1)0				•	•	ć	ć	ċ	`	: _	- 4	ŕ	ć	16.	27.	39.	2	. 00		, C. C.	136	936.	658).	6955.	4827.	3280.	1841	1 34 1	* * * * * * * * * * * * * * * * * * * *	16.33	1085.	955	843,	STORAGE	ċ	-:	-				٠ د			* *	. 00	• • • •		3	. 80	9			6.15	1267.	1679.	1199.	1124.
	0.			:	•	•	•	•	_	: _	• .	•	•	15.	24.	37.	2	1.1		• • • • • • • • • • • • • • • • • • • •	294	860.	564R.	7222.	6664	3476.	1953	1 2 5 5		2	1099	967.	853,		ċ	<u>.</u> :	_		, <sub>(</sub> ,				:		106		1		274.	282	57.3		. H. I.	1231.	1248.	1206.	1134.
	9		•	:			•			: _	<b>:</b> ,	;	œ.	₹.	<b>\$2</b> •	36.							4473	74H2.	5143	3654	2049	1363	0000	• uc 21	1113.	979.	***		•		-		,			•		7		127	173	200	265.	946	9 4	,	. 66.	1185.	1697.	1213.	1147.
	9		•	•	•	• •	ć		_	: -	<u>:</u> ,	<del>.</del>	æ	13.	23.	96	•						1344.	7723.	5377.	3834	2133				1129.	206	974.		•	e.	-					•				133		707	26.7	36.6			2	. ורוו	lans.	1221.	1156.
	0	: -		•	•	•	ċ		_		: .	•,		13.	۶.	33.		4	•	• 1 1 2	270	•	2293	7977	5540.	3006	2212.	2101	1330		1143.	1005.	R45.		•	•			•			1	2	•	8	130	1661		240	346			. 138	1073	1312.	1224.	1163.

						•	10101	101
1002	966	166	986	980	975	969	964	956
948	943.	937.	932	927.	925.	916.	911.	906
897	892	887.	883	874.	874.	869.	865.	A61.
853.	HAB.	844.	941.	A37.	A33.	829.	H26.	A22.
815,	812.	ROB.	605.	H02.	164.	796.		
			STAG	i da la				
422.A	622.8	622.A	622.B	Ī	622.8	652.8	622.R	422.A
622.A	625.8	527.A	622.A	•	622.B	622.8	622.A	522.A
422.9	622.8	622.A	627.8	•	622.8	6.25.8	622.8	622.A
627.A	625.8	622.8	627.A	Ĭ	622.8	622.B	622.A	622.A
422.A	622.H	622.A	622.8	Ĭ	422.4	652.8	622.A	622.H
527.A	622.8	622.A	622.A	Ť	6.25.A	625.8	622.A	622.8
622 . H	422.A	622.A	622.A	•	6529	6559	655.0	422.9
422.9	6.23.9	655.9	625.9	•	6.229	655.9	6559	625.4
6.664	6.55.4	422.9	653.0	•	423.0	423.0	623.0	623.0
623.1	423.1	623.1	623.1	Ĭ	623.2	623.6	623.2	623.2
F. 6 % A	623.3	423.3	623.3	Ť	623.4	623.4	623.4	623.4
A23.5	623.5	673.5	623.6	Ī	623.6	623.6	623.7	623.7
4.73.7	623.A	623.A	623.8	Ī	653.9	423.9	653.9	653.9
524.0	624.0	624.0	624.1	_	424.1	624.1	624.2	624.2
5.45.	624.3	624.3	624.3	•	4.464	4.454	624.4	624.5
424.6	454.6	454.7	624.8	•	6.424	625.0	625.0	625.1
1,25.3	625.3	4.829	625,5	Ĭ	6.25.B	6,524	626.1	625.1
626.4	624.5	426.7	6.659	Ī	627.1	627.3	627.5	627.6
427.9	624.1	62H.2	628.4	•	62A.7	658.9	629.2	620.5
630.2	636.5	430.A	631,0	•	631.3	631.3	631.3	631.3
631.3	631.2	631.2	631,1	_	631.0	630.9	630.9	630.8
43C.A	430.7	630.7	630.6	Ť	630.6	630.5	630.5	630.4
6.30.4	536.3	6.069	630,2	•	630-1	630.0	630.0	6.629
4,99,4	4.454	47.4.7	629.7	Ĭ	4.99.6	423.6	6.4.5	629.5
4.054	4.624	4.654	629.3	•	629.3	659.2	629.2	629.2
629.1	1.629	429.0	629.0	_	6.864	6,864	658.9	62A.B
624.A	428.7	428.7	624.7	_	4.86	42A.6	624.6	678.5
42A.5	628.5	628.4	62A.4	•	628.4	628.3	628.3	628.3
624.3	428.2	628.2	628.2	•	628.2	624.1		
		853. 852.8 622.8 622.8 622.8 622.8 622.9 662.8 622.9 662.8 622.9 662.9 622.9 662.9 623.1 622.9 623.1 623.1 623.1 623.1 623.1 623.1 623.1 623.1 623.1 623.1 623.1 623.1 623.1 624.0 624.0 624.0 623.1 624.0 624.0 624.0 626.1 626.0 626.1 626.0		### ### ### ### ### ### #### #### #### ####	######################################	### ### ### ### ### ### ### #### #### ####	### ### ### ### ### #### #### ########	### ### ### ### ### ### ### #### #### ####

PEAK OUTFLOW IS 8122. AT TIME 16.58 HOURS

TOTAL VOLUME	297896.	60°8	213.08	2452.	2531.
72-40UR	1034.	6,39	213.08	2052	2531.
24-HOUR	1034.	A.39	213.08	2052.	2531.
A-HOUR	3561.	7.22	143.41	1766.	2178.
PEAK	8122.	. 26.			
	CF S	INCHES	ĭ	AC-FT	THOUS CU M

MAXIMUM STORAGE = 1318.

STATION OUTING. PLAN 1. HATIO 5 END-OF-PERIOD HYDROGRAPH ORDINATES

	•	ė	•	ċ	•	•	-	:	;	•	18.	3,	<b>*</b> 6.	. 49	<b>8</b> 8.	157.	444.	1224.	5406.	11121.	7179.	5076.	2867.	1543.	1320.	1213.	1075.	957	•			•	-		·	5	7.	==	E	<b>4</b> 2.	74.	115.	157.	200.	542	201	<b>4</b> 54.	655.	92A.	1222.	1411.	2	1209.	1104.	1027.
	•	•	•	•	•	•	:	-:	÷	٥.	17.	29.	<b>4</b> 5	63.	85.	145.	396.	1137.	4584	11437.	7487.	5255.	3069	4	1330	1227.	1088.	968	•			•	-:	2.		5.	~	10.	17.	3	72.	111.	152.	196.	241.	290	<b>₽</b> 04	630.	.006	1178.	1421.	1297.	1216.	1118.	1033.
	•	•		•	•	•	1:	-:	e,	æ	15.	24.	<b>4</b> 3.	61.	82.	135.	353.	1051.	3552,	11646.	7809.	5455	3281.	1786.	1340.	1242.	1101.	979	874.	•		•	-		ě	÷	<b>.</b>	10.	15.	37.	.69	107.	148.	191.	236.	284.	392.	605.	872.	1141.	1427.	1308.	1222.	1124.	1040
	•	•	•	•	•	•	1.	٦:	e.	ņ	÷.	27.	*I*	.46	79.	127.	313.	963.	2960.	11704.	9143.	5581.	3503.	1897.	1350	1252	1114.	991	A84	!		•	-	٠,	3.	;	•	10.	:	34.	65.	103.	144.	187.	232.	276.	377.	580.	843.	1112.	1429.	131%	1224.	1134.	1047.
*	_	•	•	•	•		-		2*	7.	13.	25.	39.	57.	17.	120.	274.	R75.	2409.	11559.	8492.	5761.	3728.	2015.	1360.	1262.	1128.	1002.	468	• • •	ñ	•	.;	٠.	œ e	;	•	ě	13.	31.	62.	.00	140.	183.	227.	273.	363.	556.	. ¥15.	1087.	1425.	1131.	1215.	1150.	1055.
OUTFLOW	6	:	•	ċ	•	•		1.	٠,	7.	13.	24.	ag.	55.	75.	114.	243.	787.	2136,	11156.	8853.	5949.	395n.	2137.	1370.	1271.	1141.	1014.	906	•	STOWAGE	ċ	-	*,	3.	÷	÷	•	13.	.62	SF.	95.	135.	178.	223.	264.	350.	532.	787.	1063.	1412.	1343.	1243.	1141.	1063.
	•	•	•	•	•	•	-:	-	٠.	ċ	12.	23.	36.	54.	73.	10A.	255.	704.	1761.	10453.	9427	614A.	4169.	2764.	1379.	1241.	1155.	1026	914.	•		•	-	*.	2•	;	<b>•</b>	*	12.	.92	52.	91.	131.	174.	21A.	263	338	509.	764.	1034.	1349.	1356.	12%1.	1172.	1072.
	•	•	•	•	•	Ē	•	٦.		•	11.	22.	34.	55.	71.	102.	2º1.	527.	1392.	945A.	9867.	6360.	4401.	7345.	1349.	1251	1169.	1034	924.			•	-:	<b>:</b>	٠,	;	ů.	æ	12.	24.	52.	#1.	127.	170.	214.	259.	326	<b>*</b> # #	733.	1012.	1357.	1370.	1454.	1142.	1040.
		•	•			•	•	-		ď	Ξ.	.0.	33.	50.	69.	97.	182.	541.	1339.	A067.	10309.	560B.	4650.	2530	1411.	1341.	1193.	1050	915.	•		e e	<b>.</b> :	_:	ά.	ċ	œ.	£	Ξ.	25.	·6¶	¥.	173.	165.	200	254.	316.	465.	764.	984.	1317.	1344.	1264.	1142.	1089.
	•	•	ó	• 0	ó	•	ć	<u>.</u>	<i>:</i>	ď		19.	35.	• ₩	66.	92.	169.	492.	1285.	6671.	10734.	6885.	4816.	2676.	1497.	1310.	144	1062.	946	•		c c	¢	<u>:</u>	ď	ě.	·	Ŧ	::	2۰.	<b>.</b> 5.	٠ چ	119.	161.	205.	25%	306	445.	6.KG	<b>9</b> 26.	1270.	1344.	1277.	1201.	1094.
																																																							i

999. 991. 994. 959. 966. 991. 892. 888. 893. 993. 993. 993. 993. 993. 993			940	944. R97.	939	900	626	400
915. 910. 952. 952. 962. 962. 964. 952. 964. 952. 964. 952. 964. 952. 962. 964. 962. 962. 962. 962. 962. 962. 962. 962		6 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	106	8 0 7 °	• • • • •			8
915, 910, 901, 897, 892, 888, 888, 871, 847, 862, 892, 888, 881, 871, 847, 863, 871, 871, 872, 872, 872, 872, 872, 872, 872, 872		90 40 64 60 60 60 60 60 60 60 60 60 60 60 60 60	901.	H97.		888		880.
##1. ##7. ##7. ##93. ##60. ##5. ##5. ##5. ##5. ##5. ##5. ##5. ##		6 2 2 2 3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4	• • • • • • • • • • • • • • • • • • • •		892.		900	
# # # # # # # # # # # # # # # # # # #		6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	•===	856.	852.	948.	H45.	841.
\$\$\text{\$\		6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	824.	821.	, 918.	815.		
622.4         622.8 <td< td=""><td></td><td>4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6</td><td>STAGE</td><td></td><td></td><td></td><td></td><td></td></td<>		4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	STAGE					
622.8 622.8		# # # # # # # # # # # # # # # # # # #	622.A	•	422.8	422.8	622.R	A22.
622.8         622.9         622.9 <th< td=""><td></td><td>**************************************</td><td>622.H</td><td>_</td><td>622.d</td><td>622.B</td><td>622.8</td><td>622.8</td></th<>		**************************************	622.H	_	622.d	622.B	622.8	622.8
A22.R         A22.R <th< td=""><td></td><td># # # 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6</td><td>625.8</td><td>_</td><td>622.8</td><td>622.8</td><td>622.A</td><td>622,8</td></th<>		# # # 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	625.8	_	622.8	622.8	622.A	622,8
422.8         622.9         622.9 <th< td=""><td></td><td>\$255 \$255 \$255 \$255 \$255</td><td>622°B</td><td>•</td><td>622.8</td><td>622.B</td><td>622.A</td><td>622.A</td></th<>		\$255 \$255 \$255 \$255 \$255	622°B	•	622.8	622.B	622.A	622.A
422.4         622.4         622.4         622.4         622.8         622.8           422.4         622.9         623.9         623		622. 622. 622.	622.8	•	622.B	622.8	622.B	622.8
422.4         622.9 <td< td=""><td></td><td>622.0</td><td>622.A</td><td>•</td><td>622.4</td><td>622.8</td><td>655.8</td><td>6.22y</td></td<>		622.0	622.A	•	622.4	622.8	655.8	6.22y
422.9         622.9         622.9         622.9         622.9         622.9         622.9         622.9         622.9         622.9         622.9         622.9         622.9         622.9         622.1         622.2         623.2         623.3         623.4         623.4         623.4         623.4         623.4         623.4         624.2         624.3         624.3         624.3         624.3         624.3         624.3         624.3         624.4         624.4         624.4         624.4         624.4 <th< td=""><td></td><td>422.9</td><td>655.9</td><td>•</td><td>6.22.9</td><td>655.9</td><td>6.229</td><td>625.9</td></th<>		422.9	655.9	•	6.22.9	655.9	6.229	625.9
423.0         623.0         623.0         623.1         623.1         623.1         623.1         623.1         623.3         623.4         623.4         623.4         623.4         624.2         624.2         624.2         624.2         624.2         624.2         624.2         624.2         624.3         624.3         624.3         624.3         624.5         624.3         624.5         624.4         624.5         624.5         624.5         624.5         624.5         624.6         624.5         624.6         624.6         624.6 <td< td=""><td></td><td></td><td>6.279</td><td>•</td><td>6.25.9</td><td>6.264</td><td>6529</td><td>6529</td></td<>			6.279	•	6.25.9	6.264	6529	6529
623.2         623.2         623.2         623.3         623.3         623.4         624.2         624.2         624.2         624.3         624.3         624.3         624.3         624.3         624.3         625.4         625.4         625.4         625.4         624.8         624.8         624.8         624.8         625.4 <td< td=""><td></td><td>623.0</td><td>627.0</td><td>•</td><td>623.0</td><td>623.1</td><td>623.1</td><td>623.1</td></td<>		623.0	627.0	•	623.0	623.1	623.1	623.1
623.4         623.4         623.4         623.4         623.4         623.4         623.4         623.7         623.7         623.7         623.4         623.7         623.4         624.2         624.2         624.2         624.2         624.2         624.2         624.2         624.2         624.2         624.2         624.2         624.2         624.3 <td< td=""><td></td><td>623.2</td><td>623.2</td><td>•</td><td>673.3</td><td>623.3</td><td>623.3</td><td>623.3</td></td<>		623.2	623.2	•	673.3	623.3	623.3	623.3
A23.7         A23.7         A23.7         A23.7         A23.8         A23.9         A23.9           A24.3         A24.0         B24.1         B24.1         B24.1         B24.2         B24.2           A24.3         A24.4         B24.7         B24.8         B24.8         B24.8         B24.8           A24.3         A24.4         A24.1         B24.8         B24.8         B24.8         B24.8           A24.1         A24.1         A24.8         B24.8         B22.8		453.4	623.5	~	623.5	623.6	623.6	673.6
622.0         624.0         624.1         624.1         624.1         624.2         624.2           624.3         624.4         624		623.7	623.7	_	623.8	623.A	653.9	653.9
624.3         624.4         624.4         624.4         624.5           624.4         624.7         624.7         624.8         624.8           624.7         624.7         624.7         624.8         624.8           625.1         625.2         625.3         625.4         624.8           627.4         625.3         625.4         624.8         624.8           627.4         627.9         626.9		624.0	624.0	•	624.1	624.1	624.2	624.2
624.4         624.7         624.8         624.8         624.8         624.8         624.8         624.8         624.8         624.8         624.8         624.8         624.8         624.8         624.8         624.8         625.5 <th< td=""><td></td><td>6.454</td><td>624.4</td><td>_</td><td>4.424</td><td>454.4</td><td>624.5</td><td>624.5</td></th<>		6.454	624.4	_	4.424	454.4	624.5	624.5
K25.1         K25.1         K25.1         K25.2         G25.4         K25.4         G25.5         G25.4         G25.5         G25.7         G27.1         G27.2         G27.1         G27.2         G27.2 <th< td=""><td></td><td>474.6</td><td>624.7</td><td>_</td><td>624.7</td><td>624.8</td><td>624.A</td><td>654.9</td></th<>		474.6	624.7	_	624.7	624.8	624.A	654.9
626.0         626.4         626.4         626.4         626.4         626.9         627.1           627.6         627.7         622.8         622.8         622.4         631.2         623.2         631.2         623.2         631.2         623.2         631.2         623.2         623.2         623.2         623.2         623.2         623.2         623		6.25.1	625.2	_	4.524	625.5	4.529	625.7
427.4         627.5         628.1         628.3         628.4         628.4         629.8         629.8         629.8         629.8         629.8         629.8         629.8         629.8         630.1         630.3         629.6         629.6         629.6         629.6         629.6         629.0 <th< td=""><td></td><td>426.1</td><td>626.4</td><td>_</td><td>626.7</td><td>654.9</td><td>627.1</td><td>527.2</td></th<>		426.1	626.4	_	626.7	654.9	627.1	527.2
624.5         624.6         624.9         624.9         630.1         630.1         630.5           631.4         631.4         632.0         632.0         632.0         631.9         632.0         631.9         632.0         631.9         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.1         631.2         631.1         631.1         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631.2         631		KP7.7	624.1	_	458.4	628.6	628.8	629.0
631.7         631.6         631.9         632.0         632.0         631.9           631.7         631.6         631.5         631.4         631.3         631.3         631.9           631.7         631.6         631.5         631.4         631.3         631.3         631.2           631.6         631.6         631.4         631.4         631.3         631.3         631.2           631.6         631.4         631.4         631.4         631.3         631.3         631.2           631.7         631.4         631.4         631.4         631.3         631.3         631.3           631.6         631.7         630.4         630.4         630.7         630.1         629.7         629.7           620.5         620.4         620.4         620.4         629.7         629.6         629.7         629.6           620.7         620.7         620.4         629.1         629.1         629.1         629.1         629.1           620.7         620.8         620.8         620.8         620.8         629.3         629.3         629.3           620.8         620.8         620.8         620.8         620.8         629.8         629.8     <		624.5	629.8	_	630.1	630.3	630.5	630.B
431.7		431.6	631.9	_	632.0	632.0	631.9	631.9
K31.n         631.0         630.9         630.4         630.4         630.3         630.3           K3n.s         K30.s         K20.s         K20	•	431.6	631.5	_	631.3	631.3	631.2	631.1
630.5         630.5         630.1         630.3         630.7         630.1           630.0         620.4         620.4         620.7         620.7         620.7         620.7         620.6           620.5         620.4         620.4         620.7         620.7         620.6         620.7         620.6           620.5         620.4         620.4         620.1         620.1         620.1         620.3         620.3           620.6         620.7         620.1         620.1         620.1         620.1         620.1         620.1         620.1           620.7         620.8		631.0	630.9	•	630.d	630.8	630.7	630.7
630.0 629.9 629.8 629.7 629.7 629.7 629.6 629.6 629.6 620.5 624.3 629.3 629.3 629.3 629.3 629.3 629.3 629.3 629.3 629.3 629.3 629.3 629.0 629.0 629.0 629.0 629.0 629.0 629.0 629.0 629.0 629.0 629.9 629.0 629.9 629.9 629.9 629.9 629.3		430.5	630.4	•	630.3	630.2	630.1	630.1
620.5         624.4         629.4         629.3         629.3         629.3           623.2         624.1         629.1         629.0         629.0         629.0           624.9         624.8         628.8         628.7         628.7         628.7           624.4         628.5         628.5         628.5         628.5         628.4           628.4         628.3         628.3         628.3         628.3         628.3	_	429.0	629°H	_	6.9.7	659.7	629.6	6.629
42°,2 62%,2 62%,1 62%,1 62%,0 62%,0 62%,0 62%,0 62%,0 62%,9	_	424.5	4.629	_	6.954	6.959	6-654	6.29.3
ሉደች, የደት, የደት, የደት, የአንድ, የአንድ, የደት, የደት, የደት, የደት, የደት, የደት, የደት, የደት	_	624.2	659.1	•	629.0	624.0	629.0	628.9
529.5 528.6 528.5 628.5 628.5 528.5 528.5 628.4 528.4 628.3 628.3 628.3 628.3 628.3		624.0	628.8	_	4.8.1	428.7	628.7	628.7
528.4 628.3 628.3 628.3 628.3 628.3		628.6	628.5	_	628.5	428.5	628.4	628.4
	-	62H.4	628.3	_	628.3	624.3		

BEAK OUTFLOW IS 11704. AT TIME 16.42 HOURS

TOTAL VOLUME	405980.	11496.	11.43	290.39	2196.	3449.
72-H00R	1410.	• 0 •	11.43	290.39	2796.	3449.
24-HOUR	1410.	, 0,	11.43	290.39	2796.	3449.
6-HOUR	4903.	139.	46.6	252.53	2431.	.6662
PEAK	11704.	331.				
	CFS	CMS	INCHES	I	AC-FT	THOUS CO M

MAKINUM STORAGE # 1429.

STATION OUTING. PLAN 1. RATIO 6 FND-OF-PERIOD HYDROGRAPH ORDINATES

	ė	•	•		•	:	-		11:	20				24.5		. 200			4734	1504 1.	22684.	14474.	. 7266	4447	2440	740	3.46.	9000	1262				-		, ,	ć		15.	22.	37.	94	151.	224.	305.	415.	544.	695.	1011.	1270.	1366	1535.	1781.	1514.	1364	
	•	•		•	~		-		10.	27.	, (r)	8		346		100	• • • • • • • • • • • • • • • • • • • •	2020	9761	13211.	23430.	15090.	10204.	5370.	2577.	100	1366		1001	• • • • • • • • • • • • • • • • • • • •			-	2.	•			*	21.	34.	80.	144.	217.	290.	402.	534.	675.	973.	1255,	1359.	1478.	1605.	1538.	1361.	
	e e	•	•	ċ			: -		•	25.		***	7			7 7 6	• • • • •		4305	11497.	23004	15794.	10555.	5788	2750.	16.24	1 252				1139.		•				•	•	20.	31.	7.	137.	<b>500</b>	7.8.8	390.	521.	657.	937.	1738.	1352.	1435	1823.	1550.	1392.	
	•	•	•	•	-:	1.	: :		£	22.	, <u>, , , , , , , , , , , , , , , , , , </u>	80.	127.	220				9 501	MAGD.	1111	24 300.	16538.	10907.	4217.	2.461.	1001	1360		1224	100	1146.		٥	~	;	•		13.	19.	29.	64.	136.	202.	275.	378.	507.	. 2. 4. S	905.	1220.	1344.	1410.	1933.	1584.	1404.	
3	•	•	•	•	0	1.	-		7.	20.		74.	127.	100	203	3			86.09	10701	54264.	17327.	11243.	6690	3188	1785.	1367.		. ACC.	16.70	1154.	يي		2.	•		•	13.	6.	27.	63.	123.	104.	271.	366.	404.	628.	844.	1198.	1335.	1397.	1932.	1610.	1416.	
OUTFLOW	ċ	•	•	ċ	6	-	-		7.	. 8.	-	7 .	1.6	47	340				1351	10497	2-1A3.	14165	11659.	7211.	3472	H76	1174		1246		1161.	STORAGE				·			18.	ξ.	58.	117.	187.	263.	355.	• BO.	614.	834.	1173.	1325.	1390.	1417.	1634.	1429.	1
	÷	•			•	-	: -:		÷	17.	8	2	-		3 4 6		• 60 %		100	10374	22/92.	19050	12154.	7745.	1641		1.81			• • • • • • • • • • • • • • • • • • • •	1155.		ě	-		,		12.	17.	25.	53.	110.	184.	254.	344.	467.	£01.	802.	1146.	1315	1346.	1785.	1664.	1444.	ı
	•	•	•	•	•	-	: _:	-	S	15.	35.	, y	1.5	12.	306			20.20	• 1 1 1	102.17	21274.	10970.	12662.	8713.	36.50	7, 7	1 348		1257		1177.		6	-					17.		* 6	104.	172.	244.	333.	454.	SA4.	112.	1116.	1305.	1342.	1736.	1694.	1460.	,
	e e	;	ď	c		_	_	-	٠,٠	]3,	-		96.	166	400				7.396	10040	10301	20005	172A9.	A753	4574	. 616	1394	75.5			1144.		6	:_:	,			~	16.	23.	**	ě,	165.	240.	323.	***	574.	744.	1047.	1294.	1377.	1675.	1724.	1477.	!
	ċ	•	ċ	ć	ċ	-	· -	-	ų	12.	<u> </u>	6	90	3.0	28.3					* 1 × 0	17190	21473.	13797.	9393.	45.62	2112	1629		1264.				<u>.</u>	<u>:</u>	٠,	•		10.	15.	23.	<b>*</b> 1.	92.	15A.	232.	314.	427.	561.	714.	1044.	1282.	1372.	1605.	1754.	1496.	j

1220.	1092.	1025.	988	954	924.			625.8	622.8	622.8	622.B	6559	6529	655.0	623.n	623.4	623.8	624.3	65479	625.6	4.929	627.4	629.2	631.0	631.6	632,3	634.2	632.6	631.7	530.7	430.0	629.6	629.3	629.1	654.6	
1237.	1102.	1029.	992	95A.	927.	900		622.8	622.A	622.H	622.4	422,9	655.9	655.9	623.0	423,3	623.B	524.3	624.A	625.5	4.929	427.2	6.99.0	630.9	431.5	635.0	634.3	632.A	A31.A	4.0F.A	6.30.0	6.654	4.664	424.1	679.0	62A.A
1253.	1112.	1035.	995.	961.	430.	903.		6.22.8	6.23.8	622.4	622.8	6.22.y	4.55.4	622.9	623.0	623.3	673.7	5.4.9	K24.7	4.654	6.26.3	627.1	628.8	K30.7	413.5	4.11.9	4.454	435.9	6.11.8	4.0EA	630.1	4.679	4.624	4.29.2	0.464	628.B
1270.	1173.	1049.	666	964.	913.	995.		622.8	622.A	822.8	622.8	6529	6.229	655.9	623.0	623.2	627.7	6.450	624.7	624.3	624.2	627.1	6.8.6	630.6	631.4	631.4	4.464	633.1	4.11.4	631.0	6 30 . 2	629.7	4.629	420.5	6.054	628.8
128A.	1134.	1646.	1002	96ª.	<b>934</b>	90A.	STAGE	622,B	622.4	642.8	627.A	655.9	6529	6529	623.0	623.2	623.6	624.1	624.A	6.25.2	625.1	627.0	4.829	630.5	631.4	631.R	634.3	633.2	632°n	631.2	630.2	659.7	4.629	429.2	629.0	629.8
1306.	1148.	1052.	1005.	971.	439.	910.																														428.9
1324.	1162.	1059.	1000	474.	447.	913.		422.8	622 A	622 A	627.A	622.0	622.0	6.229	423.0	623,1	623.5	524.0	674.5	625.1	6529	624.A	67H.0	630.1	431.3	431.7	633.4	633.5	632.2	4.16.4	430.4	6.29 B	624.5	424.2	429.0	6.654
1347.	1175.	1047.	1011.	97A.	944	916.		622.B	622.A	A 2 2 A	422.4	A22.A	427.9	622.9	6.53.0	623	623.5	454.0	A.24.A	625.0	4.25.A	426.7	427.8	6.624	431.2	431.7	633.4	633.7	632.1	431.5	430.5	629.A	629.5	K.29.3	429.1	424.9
1355.	1199.	1075.	1017.	obl.	944.	914.		622.8	627.B	622.B	622.8	4.7.7	655.9	6529	623.0	623.1	673.4	623.9	674.4	625.0	625.7	626.6	627.6	524.7	431.1	7.164	533.0	633.9	432.4	6.11.6	634.6	6.964	. 5°664	624.3	h29.1	6.854

1005. 1001. 905. 905.

PEAK OUTFLOW IS 24300, AT TIME 16.42 HOURS

TOTAL VOLUME	949477.	26835.	26.74	679.09	6539.	8065.
72-H0UR	3297.	93.	26.74	479.09	6539.	<b>8</b> 0.65.
24-HOUR	3297.	93.	24.74	619.09	6439.	A165.
4-HOUR	11707.	332.	73.74	442.91	5805.	7161.
PEAK	24390.	688.				
	SES	SMO	INCHES	37	AC-FT	THOUS CU #

PEAK FLOW AND STORAGE (EMD OF PERION) SUMMARY FOR MULTIPLE PLA! "RATIO ECONOMIC COMPUTATIONS FLOW AND STORAGE FLOWS IN CURIC FEET PER SECOND (CUMIC WEYERS PER SECOND)
AREA IN ROUARE MILES (SQUARE K), CAMPITERS)

OPF PAT I ON	STATION	AREA	PLAN	RATIO 1	RATIO 2	RATIOS APPLIEN TO FLOWS RATIO 3 RATIO 4 RAT 30 .40	1. 1ED TO FL PATIO 4	.0WS .8A710 5	PATIO 6 1.00
HYBPOGRAPH AT	INFLOW		-	193.	386.	579.	773.	966.	1932.
ROUTEn TO	0011%6	. 17	-~	99.	344.	535. 15.16) (	720.	902.	1802.
47096694PH 47	INFLOW	.06	~~	1.86) (	131.	197.	263.	328.	657.
2 COMMINED	-	. 23	~~	135. 3.A?) (	13.051	710.	953. 26.99) (	33.90) (	2391. 67.71) (
OAUTES TO	0011146	. 23	~~	31.	3.471	542. 15.36) (	A15. 23.08)(	1091.	2278.
MYDROGRAPH AT	INFLOW	1,51	~~	1052.	2104. 59.581(	3156.	4208.	5261.	10521.
POUTED TO	9011 is	3.91)	~~	274.	1667.	2561.	3416.	4270. 120.911(	8540. 241.821(
HYDAOGRAPH AT	INFLUW.	1.461	~~	556.	31.5116	1669.	2225. 63.01)(	27A2.	5563. 157.53) (
AOUTED TO	0UT146	1.96)	~~	130.	817.	1444.	1933.	2414.	4811.
HYDADGRAPH AT	INFLOW	2.13 5.52)	~~	1646.	3292.	4937.	6583.	8229. 233.02) (	16458.
4 COMPINED	~	4.59	<b>~</b> ~	1914.	5303.	884°. 250.33) (	11840.	14742.	29409.
ROUTED TO	0UT I'NG	4.59	~~	186.	1229.	4134.	6122. 229,99) (	11704.	24300.

SUMMARY OF DAM SAFETY ANALYSIS

	TIME OF FAILURE MOURS	000000
TOP OF DAM 702,70 51.	TIME OF MAX OUTFLOW HOURS	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	DURATION OVER TOP HOURS	1.25 4.25 5.75 6.58 7.00
SPILLWAY CPEST 690.78 0.	MAXIMIM OUTFLOW CFS	99. 344. 535. 720. 902.
. VALUE 78 0.	MAXIMIM STORAGE AC-FT	
INITIAL VALUE 699.78 0.	MAKIMUM DEPTH OVER DAM	2.1.1.0 2.0.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.
ELEVATION STOWAGE OUTFLOW	MARTPUM RECEPVOIR M.S.ELEV	703.07 703.69 703.63 704.15 706.35
PLAM 1	RATTO OF PMF	
PLAN		

COMPUTER SUMMARY AURKSIS . LAKE ELEWAR

	TIME OF FATLURE HOURS	000000
TOP OF DAM 674.80 33. 88.	TIME OF MAX OUTFLOW HOURS	11 11 11 11 11 11 11 11 11 11 11 11 11
	DURATION UVER TOP HOURS	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
SPILLWAY CREST 671.02	MAXIMIN OUTFLOW CFS	31. 121. 542. 815. 1091.
V4LUE •02 0•	MATININ STORAGE AC-FT	######################################
INITIAL VALUE 671.02 0.	MAKIHUM DEPTH OVER DAM	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
FLEVATION STOWAGE OUTFLOW	MBXTMIN WESEPVOTS W.S.ELEV	673-17 675-13 675-69 675-95 676-16
	RATTO OF PMF	
:		•
3		

LAKE MERON GWENTER SAMMEN KUNLISK

## SUMMARY OF DAM SAFETY ANALYSIS

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	TIME OF FAILUNE HOURS	
10P OF DAM 658.20 142. 155.	TIME OF MAX OUTFLOW HOURS	11 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
		3.55 2.55 2.55 2.55 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1
SPILLWAY CREST 650,30 0.	MAKIMIN OUTFLOW CFS	274. 1867. 2561. 3416. 4270.
VALUE 0.00	MAXIMIM STORAGE AC-FT	159. 203. 266. 288.
INITIAL VALUE 650.30 0.	MAXIMUM UFPTH OVER DAM	2.93 6.93 6.93 13.76
ELEVATION Storage Outflow	RESERVORA N.S.ELEV	659.03 661.11 662.45 663.73 665.01
	0.4.110 0.7.10 PHF	
F 18		

SUMMARY OF DAM SAFETY ANALYSIS

	TINE OF FAILUME MOURS		 	0.00
TOP OF DAM 655.20 69.	TIME OF MAX OUTFLOW HOURS	14.17	14.17	14.17
	DURATION OVER TOP HOURS	4.02 8.03	10.33	11.58
SPILLWAY CREST 64M.07	MAXINUM OUTFLOW CFS	130. 817.	1444.	2414. 4811.
INITIAL VALUE 648.07 0.	MAXIMUM Stopage AC-FT	A3.	124.	143.
INITIAL 648	MAXIMUM DEPTH OVER DAM	1.24	6.61 5.30	5.98 9.37
FLEVATION STAPAGE OUTFLOW	MAKIMUM MESFRYDIR M.S.ELEV	554.44 558.14	659.H1	664.57
	PATTO 05 P45	- ×	€ ¢	1.04
P. P.				

LAVE BOUNDED CONFUTER SAMIES

## SUMMARY OF DAM SAFETY ANALYSIS

	TIME OF FAILURE MOURS	00000
TOP OF DAM 629.60 1031. 1647.	TIME OF MAX OUTFLOW HOURS	24.00 14.58 17.17 16.58 16.42
·	DURATION OVER TOP HOURS	0.00 3.00 4.64 7.67
SPILLWAY CREST 622.80	MAKIMIM OUTFLOW CFS	186. 1270. 4138. 8127. 24309.
INITIAL VALUE 622.80 0.	MAXIHUM Storage ac-ft	470. 930. 1171. 1318. 1429.
INITIAL 622	MAKINUM DEPTH OVER DAM	00 - N
ELFVATION Stohage Outflow	MAKIMUM MESEPVOIR M.S.ELEV	628.02 631.34 631.34 631.34 631.49
	HAT10 OF P4F	0 5 7 7 9 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
PLAN		•

LAKE SMERLOOD
CANTITEE SMMARY ANNISO